

Lectures notes

On

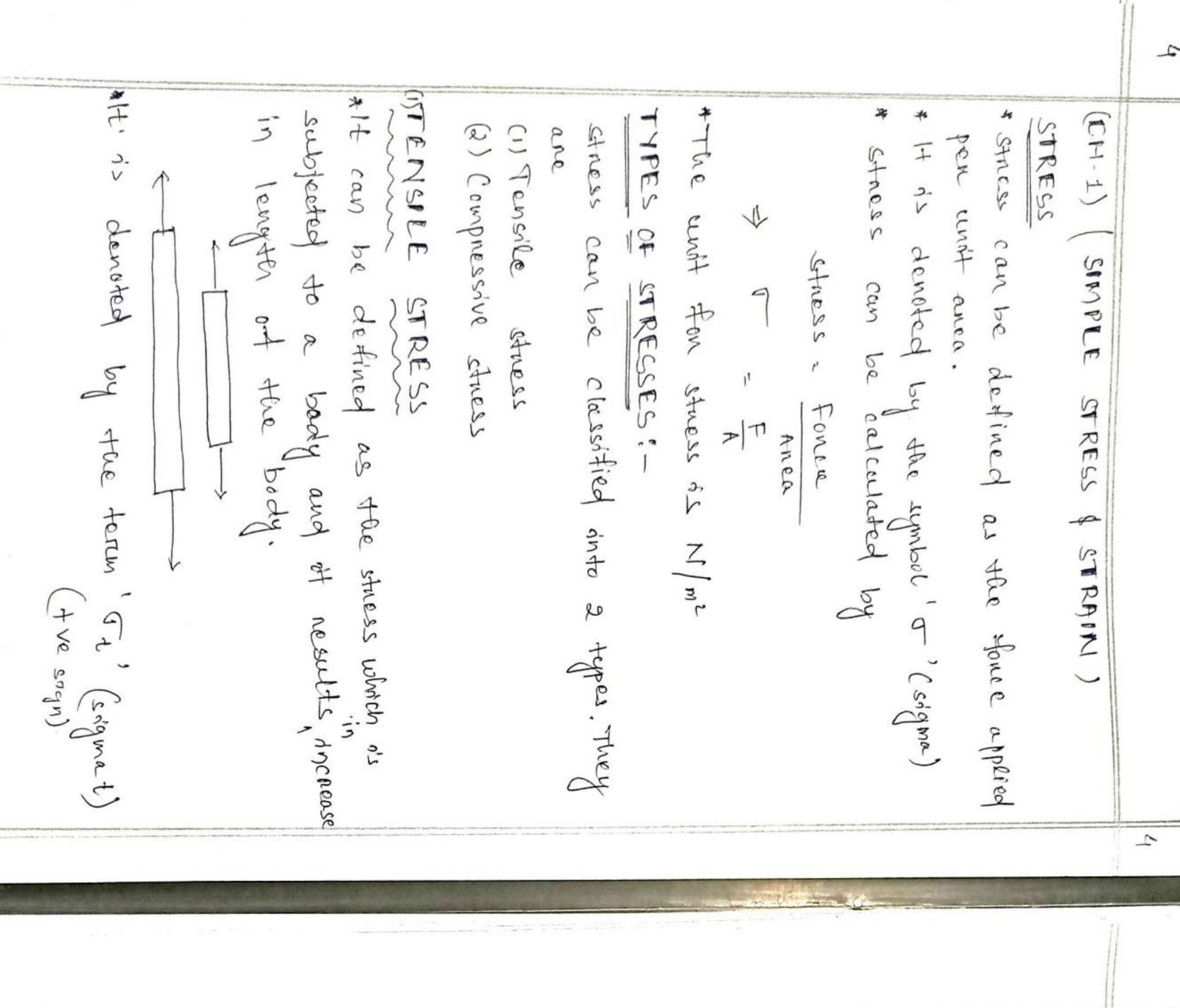
STRENGTH OF MATERIALS

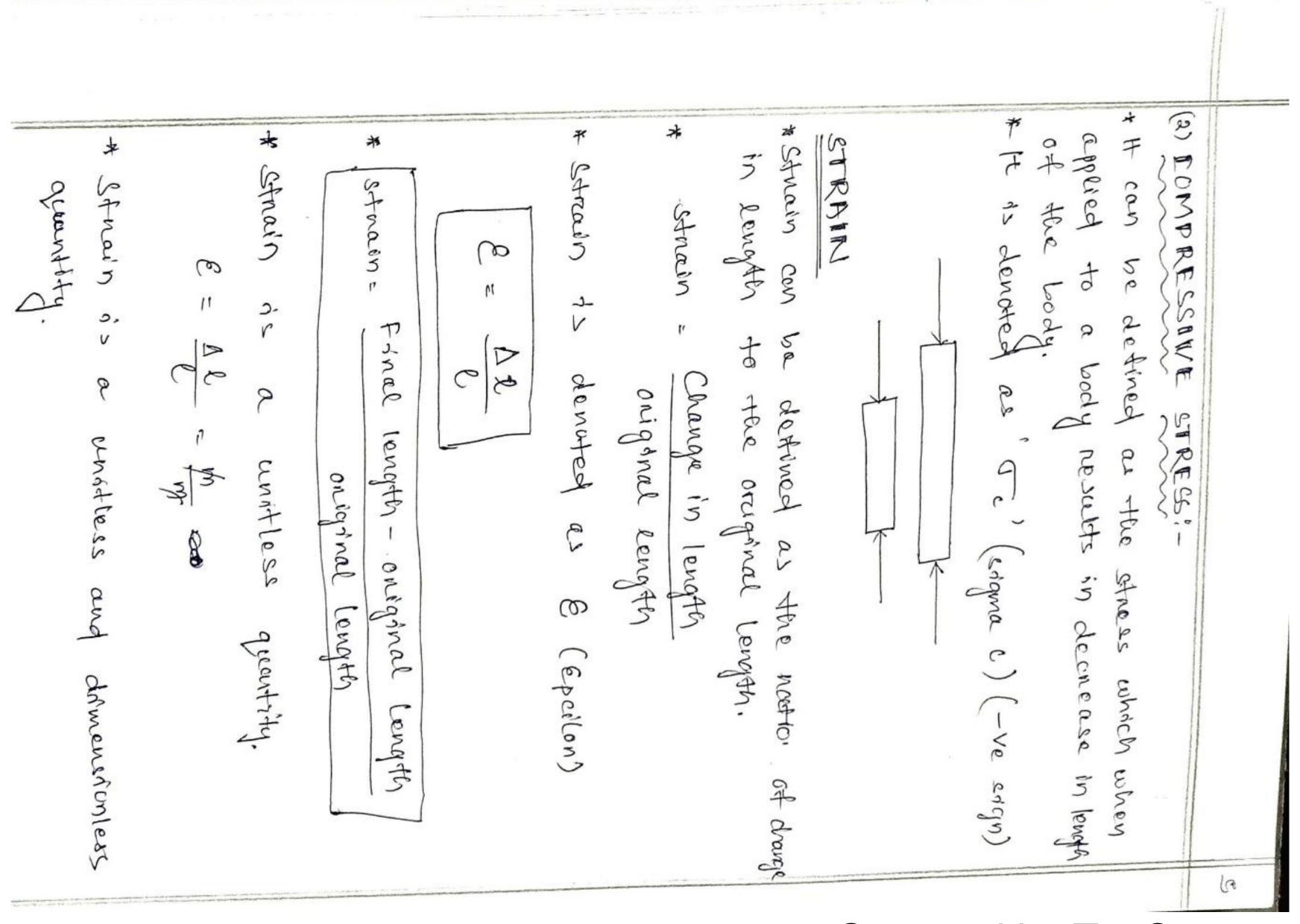
Course Code-TH2

Prepared by

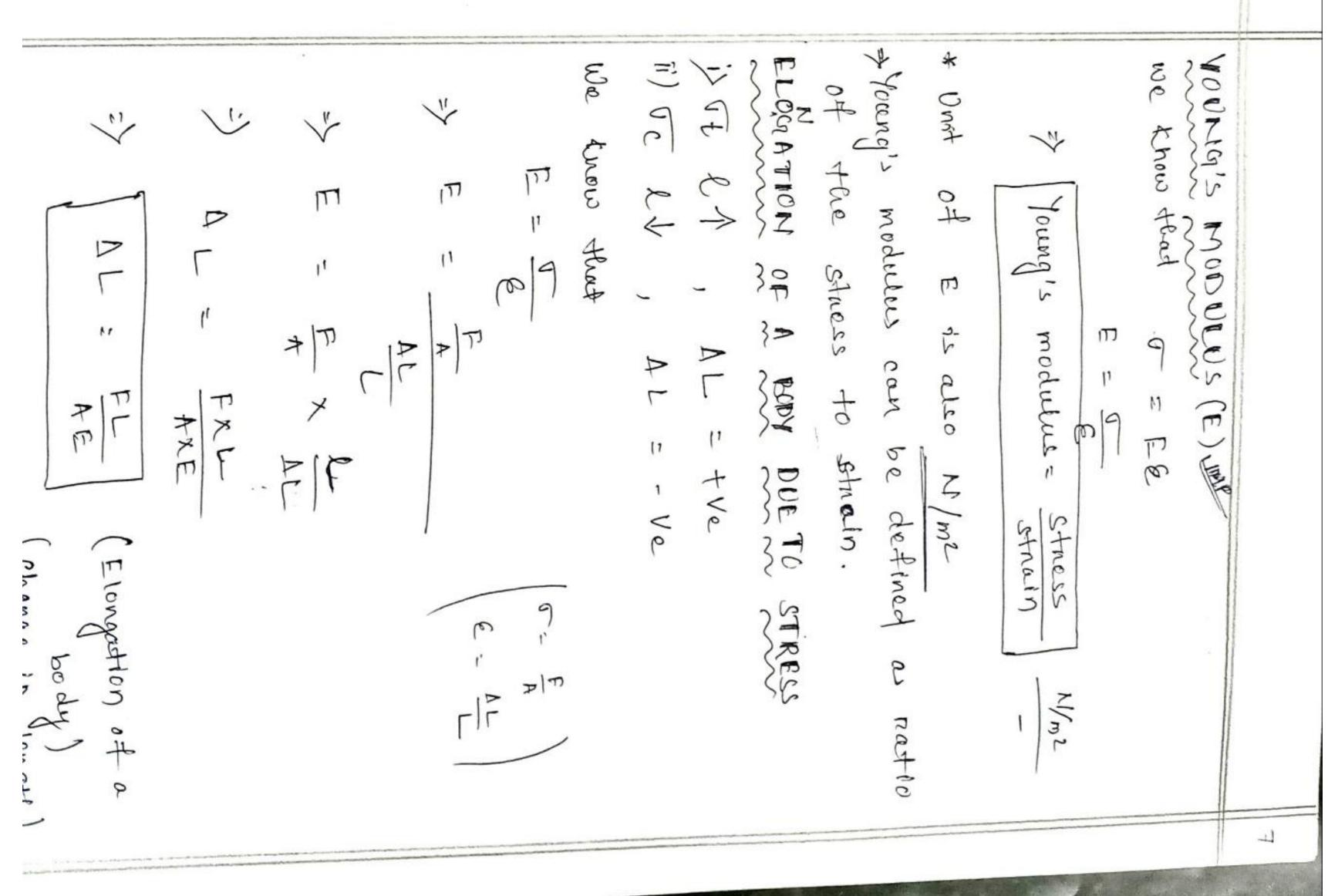
Mrs.Shradha Suman Adabar

Department of Mechanical Engineering

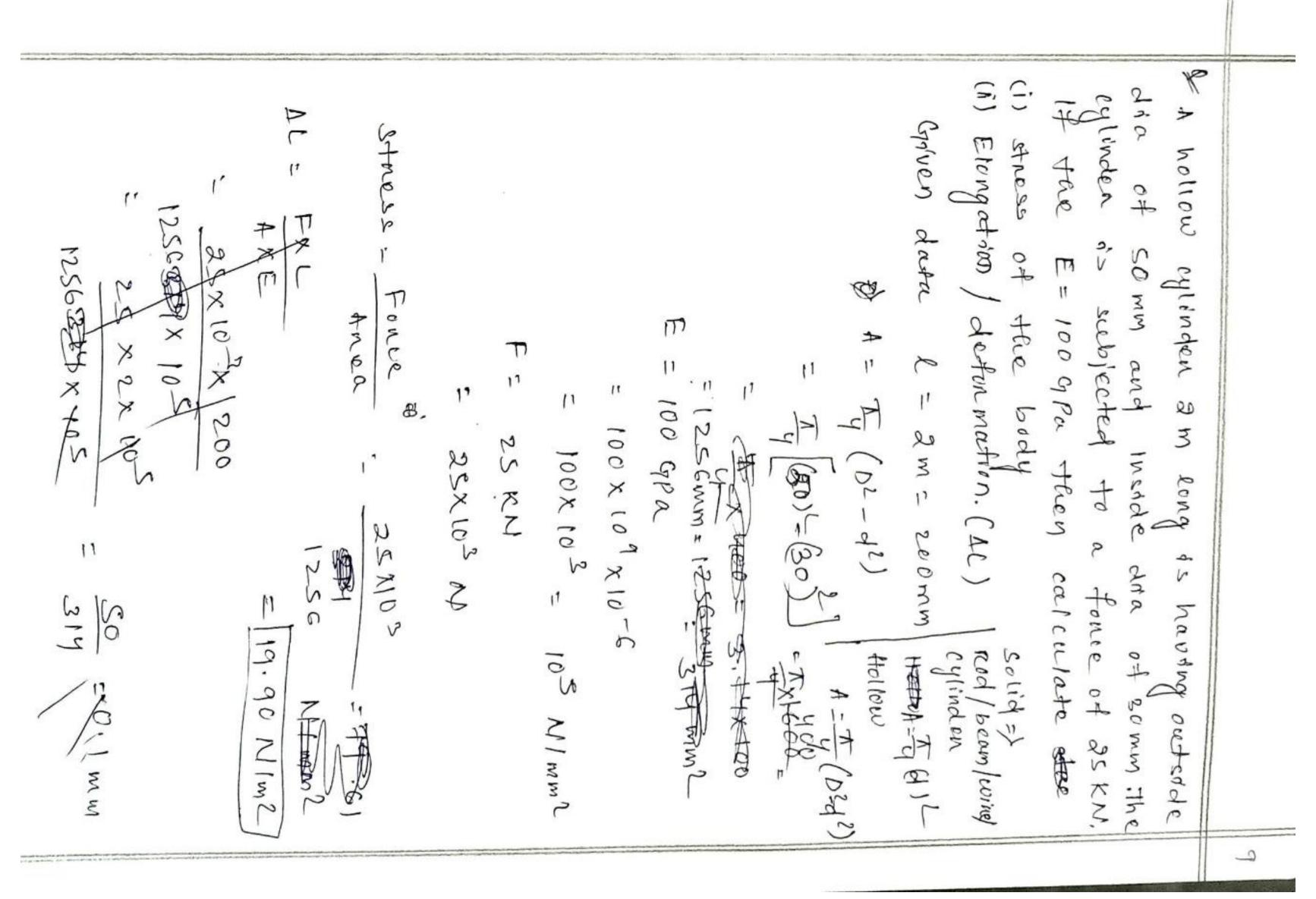




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touce of 40 KN. 200 cy Pa cf the choss-section gaven!-41 poor 十八日 2007 7 5 4 OIXH X 00 h 400 x 2 x 10 5 4 × 10 4 × 10 3 steel nod 6 = 401 X82 × 1000 Cascalate tax extengation to (ong and serman 20x20mm) 1 m = 1000 mm 402103 20× 10 9× 10 -6 200x 10 3 M/mmg-30× 20 mm=480mm2 2RIOS MIMM2 4 x 10 4 N LWW 5.0 = 20x 20 mm

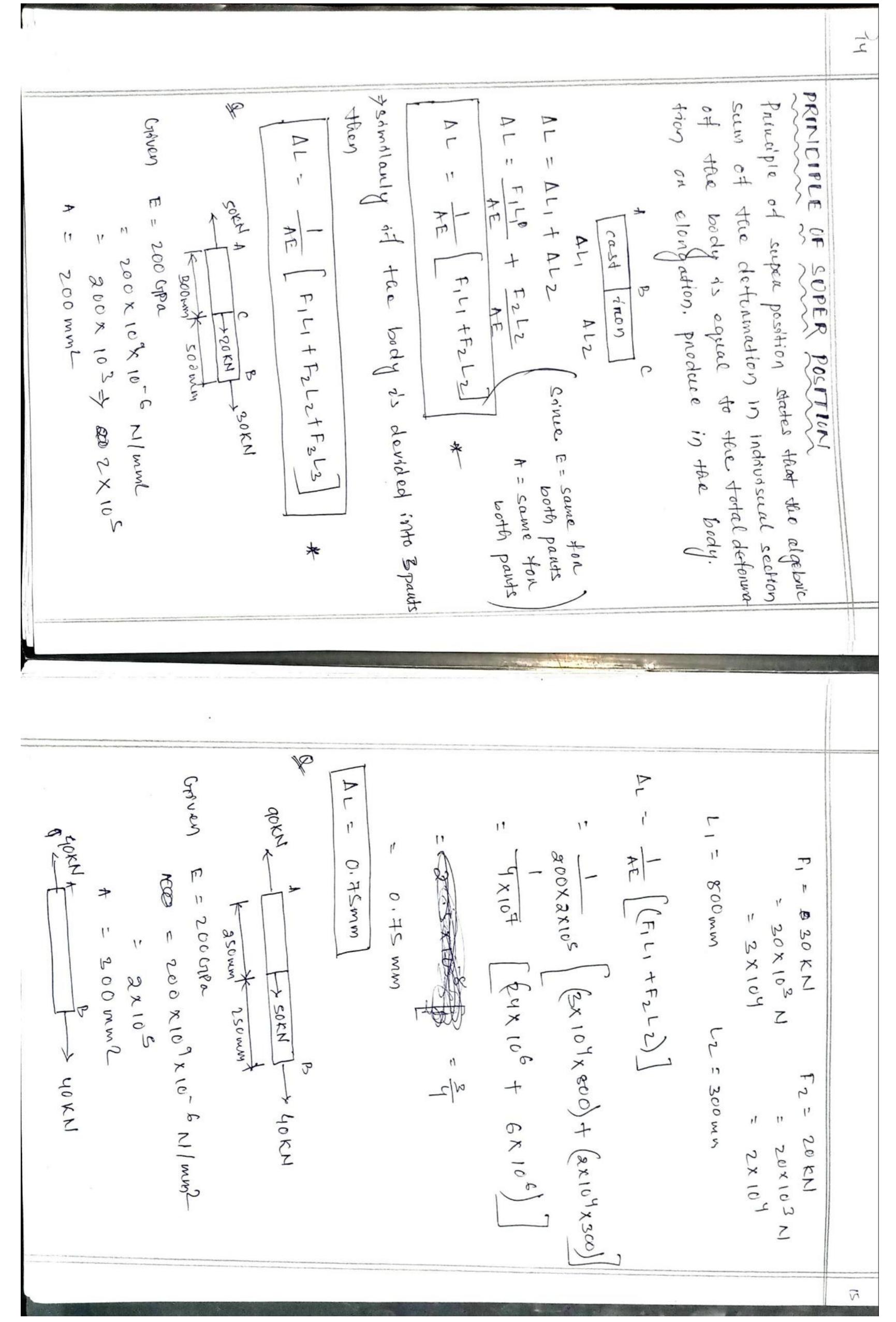


d= \(\frac{50}{4} \times 4\)

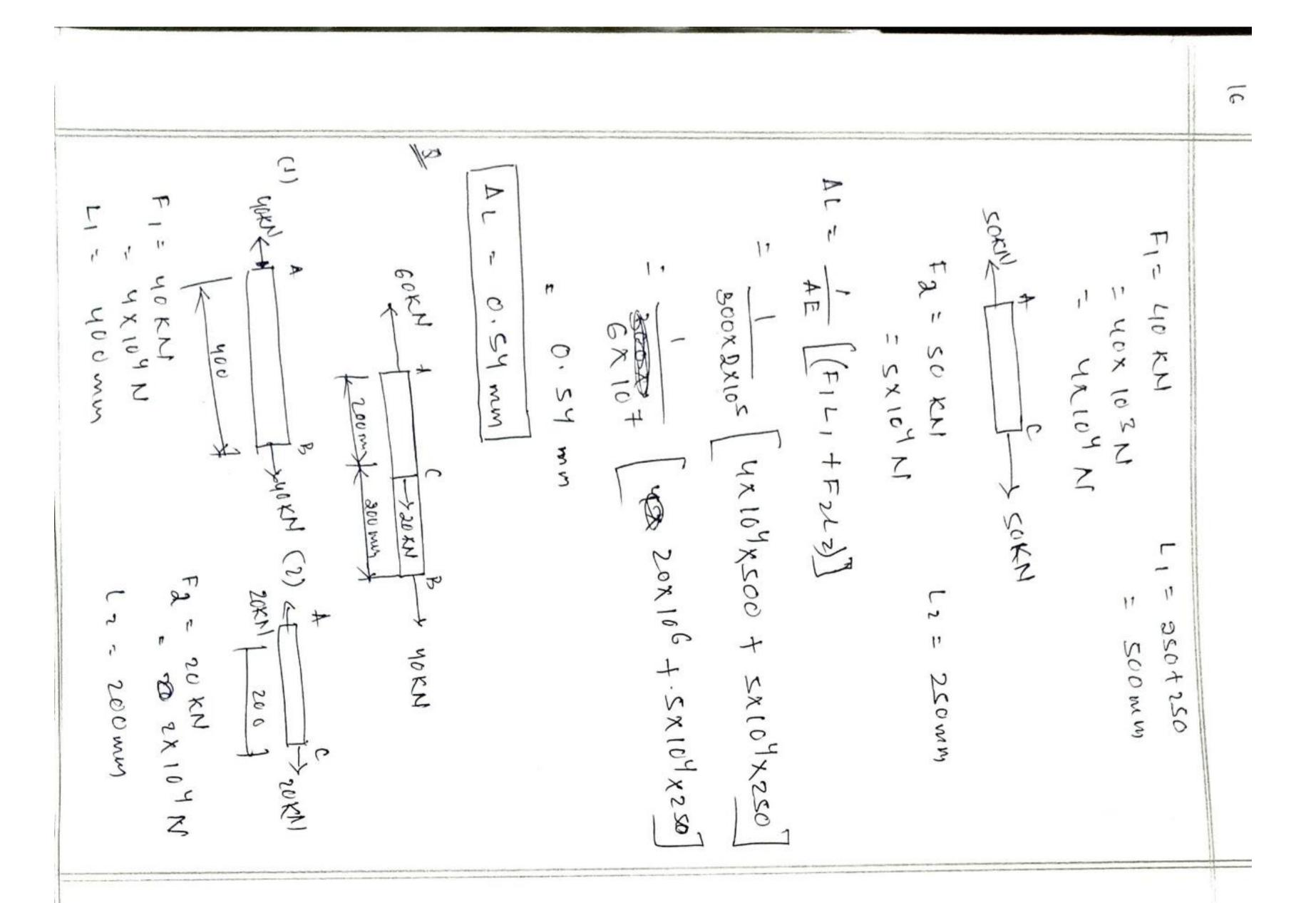
= \(\frac{300}{3.14}\)
= \(\frac{300}{3.14}\)
= \(\frac{300}{3.14}\)
= \(\frac{300}{3.14}\)
= \(\frac{300}{300}\)
\(\frac{4}{300}\)
\(\frac{300}{3.14}\)
\(\frac{1}{3}\)
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\(\frac{1}{

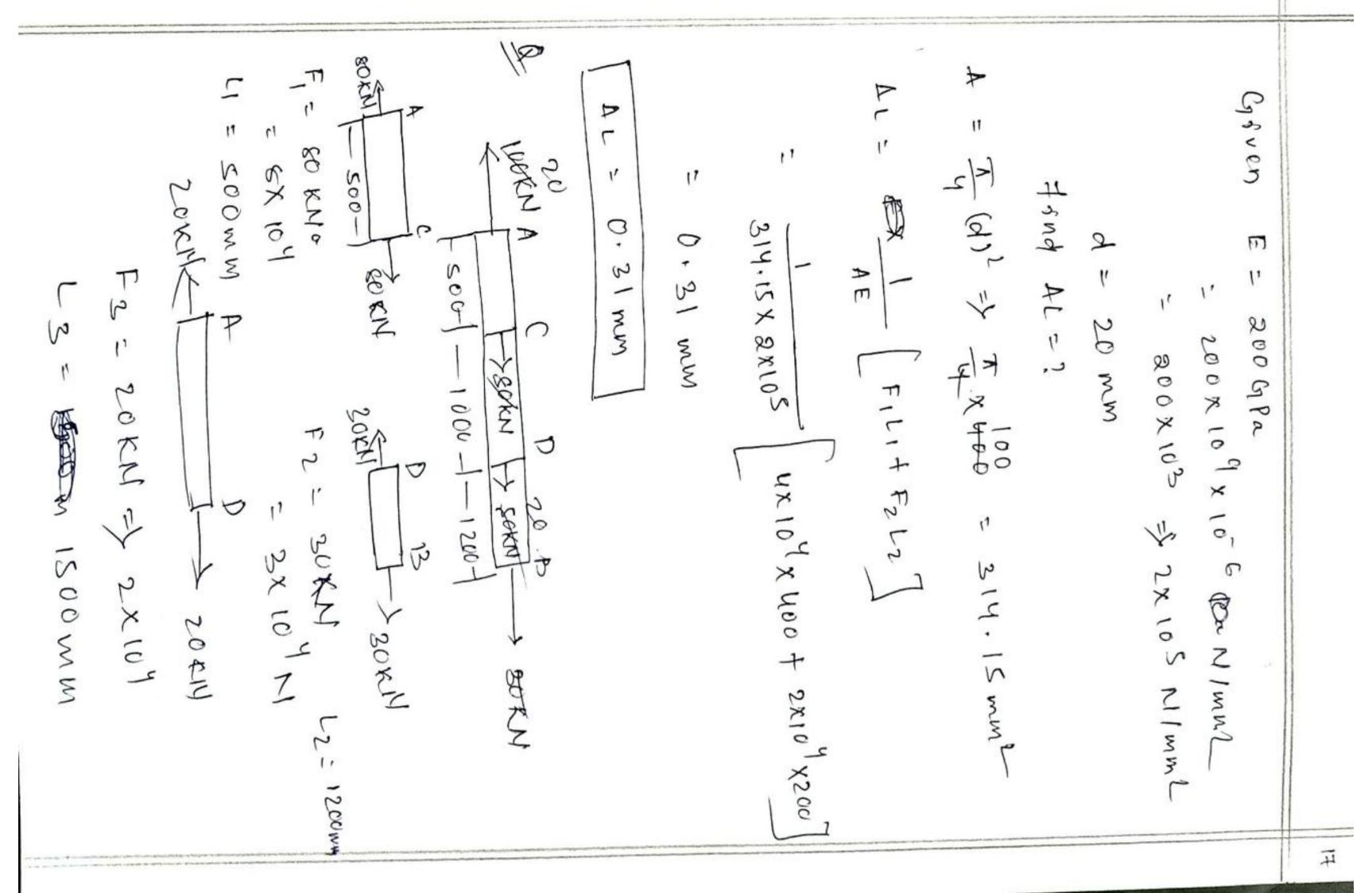
 $A = \frac{\pi}{4} (02 - d2) = 2500$ $\Rightarrow \frac{\pi}{4} ((120)^{2} - d2) = 2500$ $\Rightarrow 120^{2} - d2 = 3500 \times 4$ $\Rightarrow 14400 - d2 = 14400 - 4456.23$ $\Rightarrow d = \sqrt{99.71} \text{ mm}$ [d = 99.71 mm]

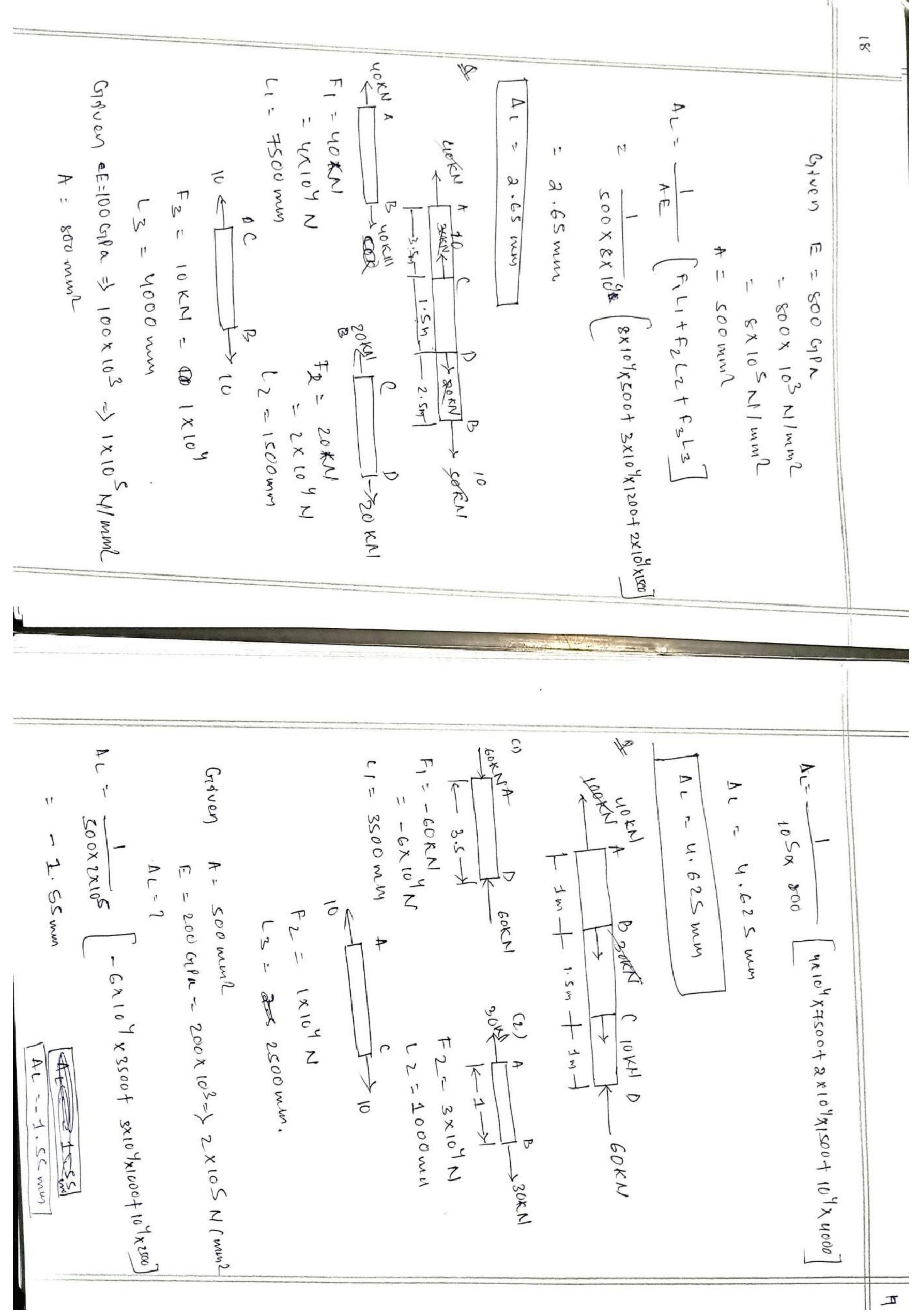
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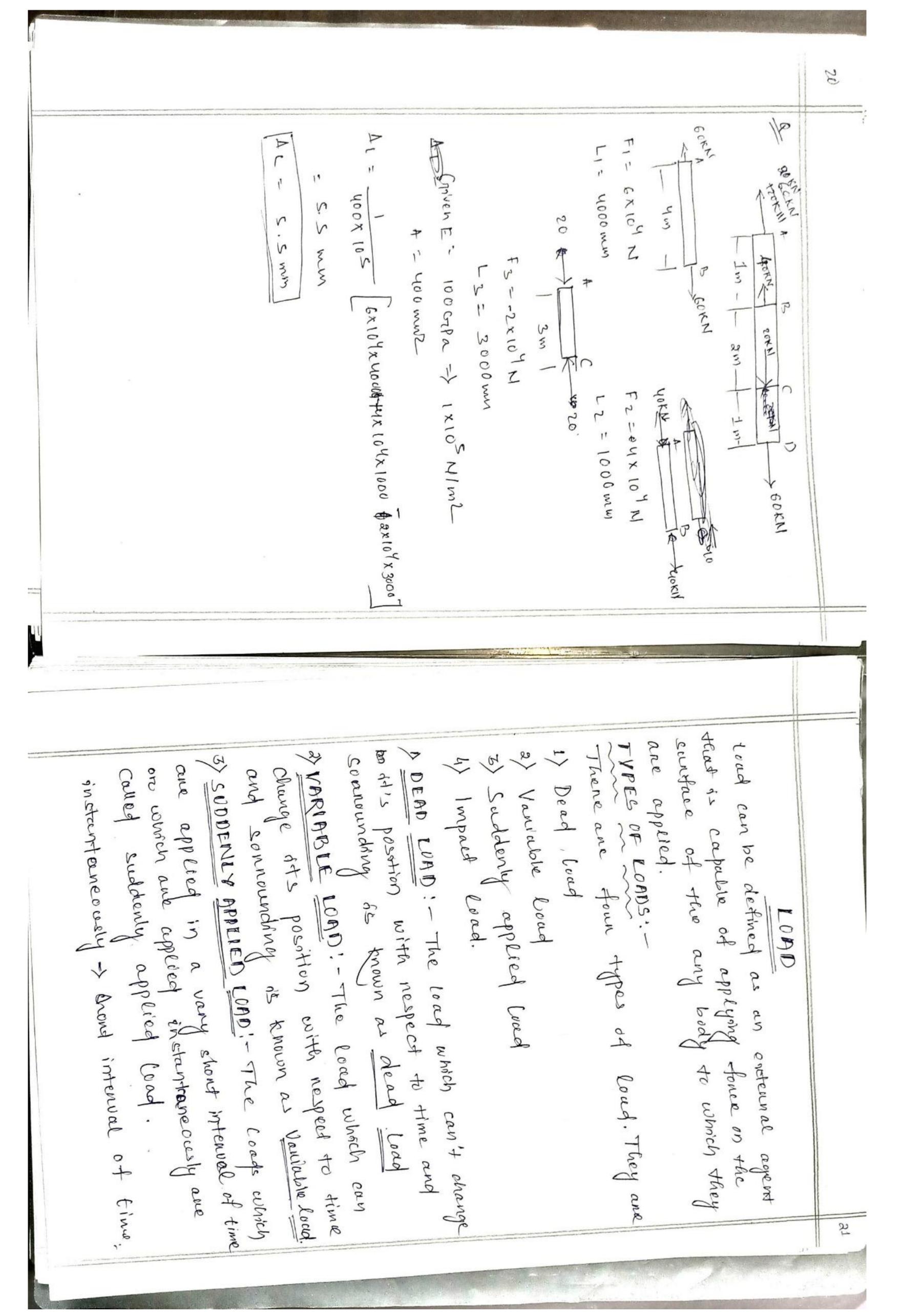


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e than one of the section destined as the section one section one material. SECTION:- Material -2 Material -2 E2 = 72 E2 = 72 E2 = 72 E3 train one Same ton boots. The material.	IMPACT LOAD! The load instral velocity is called enti- castebring of a ball velocity. Composite section can be a material. STRESSES IN CompositE SETTION! (Mone Ra Material & E = T E1 = T E1 = T Material & Material & Material & Material & Material & Material & E Material & E Material & Material & Material & Material & E1 & E2 Strange Sent Sent Sent Sent Sent Sent Sent Sen
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6 steel bours having cross-sectional carea of so mm. Calculate the load on the column it the streets of the concrete is given z.c.m. Anea of EC material the natio of marterital 2 force off on composite section (F) 11 of concrete gives; anea steel = 11 300 mm 50000 mml young's modules of steel T 3.5 N/mm2

concrete = Total anca -

49500 mm2

2.5 X18

Area of single steel = 7 d2

7 x(25)2

490.87 mm2

Dra of steel (d) = 25 mm

500 X600 -

250000 mm2

05 As + 63x500 + 49500x 3.5

free of all seed now: 4 x 490-87

EC = 149Pa = 2109Pa= 210 x 10 9 x 10-6 gIUXIUZ NImme THX109 XLES 14×103 NImm

Area of concrete = Total anea -Total Force (F) - 1000 A 1000×103

250000 -

1963.48

minh

Choss-seestional contains 4 speel bur. The

total fine of the section is given 1000 KM Taken Es= 210 Gpa and Ec= 14Gpa. striess in the concrete and steel laws if the Dasta griven:

of each steel ban is 25 mm. Calculate the rectangular colaumn 500 X 500 mm

=> 03 = 02 x Es => 05 = 06 x 340 x 105 => F = F1 + F2 => F = 05 + 5 + 02 + 24 8036.526 = 29452 - 3502 + 24 8036.526 = 29452 - 3502 + 24 8036.526 = 3.60 M/mm² => 05 = 1500 => 1500 x 10³ => 05 = 1500 => 1500 M/mm² -> 1500 M/mm²

diameter each. Calculate the acts sthoss A square column having 400mm x 400mm in ca section contains 6 steel bans having 15 , steel and concrete if Es= 2000/Pa an Ec = 209Pa and total fonce = 150 KM Inea of concrete = Total area Total Anea: 400 x 400 Dra of steel ban(d) = 15mm Amea of steel ban = 79 (d)2 Gavery docta:-Total area of steel bour = 2000 Pa = 200× 104 20 Gpa -000001 159293.16 mm 20×109×10-6 2007103= 20171051 P8-30F -80×103 2 x 10 4 N/mm/ = = 176. 7 = 160000 mmL 14.341 x h mm 48.904

Anea of concrete: Take the young's modules of concrete is it. Anea of seel - 7 (d) xy Gaven data! - 0 = 400 mm concrete having 200 mm drameter each. Find of OSAS + OCAC 120×1256.63 f 5×124407-07 77 282 O. 95 mm N column 400 cm dsamester 125663.7 - 1256.63 Total Anea- Anea of 124407. 67 mm. 17 CX00 A x (20)2x 4 7 x(400)2 1266.63 has 4 so

Calculate

ā.

the total

force on

disameter of each

steel and is 25 mm

concrete and

the stress 19 the

steal ban given data! -Ec-14 Gpa. A Nea of Section 500x 500mm concrete = Acel 001 T. A = 500 x 500 mm Total Anea. Anea of the 250000 - 490-87 79×103 249509.13 mm 14.28G Xar 1/28/25/2 25mm @ 490.87 mm 2 25 00 00 Ec: 14 GPa = 14× 10 ×mm 200 Ry Pa 200× 103 N/mil 163×103 2x1USN/my 10p

s when the budy is subjected to tensile st the length of the body is inchease where the budy is subjected compressive stress the budy is subjected compressive stress the budy length of the budy decreases > when a TEMPERATURE STRESS / THERMAL STRESS: Almpenasture stress. contractor than a stress is in stries on calculate of from this med and this gress is known as thermal An Yeald - de-form - change in shape and size PLERSIPE LIRES 17 SINPLE BIRS! 106 95-150C etuess on (1500 x 196378) + 80 x 2480 29452.20cf 248036.520c 15 x 3.6 = 54 M/mmn2 277 - 88 HTF5 mm/N 03.5 = 24.88 htt B a stress or Induced in the simple. bans, Thennal any expansion

Q = 12 × 10-6 / C Yould is goven Im. Take E= 200 GPa and Data given :- length of nod = Q=12×10-6/0C 12X10-6x40 -(A) yield = 1 mm 62.66 N/mm auogpa 200×103 M/mml 1- 40°C 6000 5 mg × 200× 103 6000 mm 6×1000

10

the thermal stress devolved in the ban 14. nod of 6m a fax al the both and. It is Xt E 17 x 10 - 6 × 90 × 103 x + 50 5 17 x 10 - 6 x 90 x 10 3

respectively. Data gover 1 = 158 = 12×10-6/K = 200 × 103 M/mm2 200.012

O NITE 12×10-6×15×200×10-3

I A steel ban as heated to a (ii) Hield case / take A-2mm SOK. Calculate the thenmal steel ban . Take given: = 50 K 12×10-6 K S m = SX1000 = 5000 Q = 12 X 10 6 K, 0 200x 103 N/mm2 stress tempenatione induce

through 15K. Calculate the shress devel

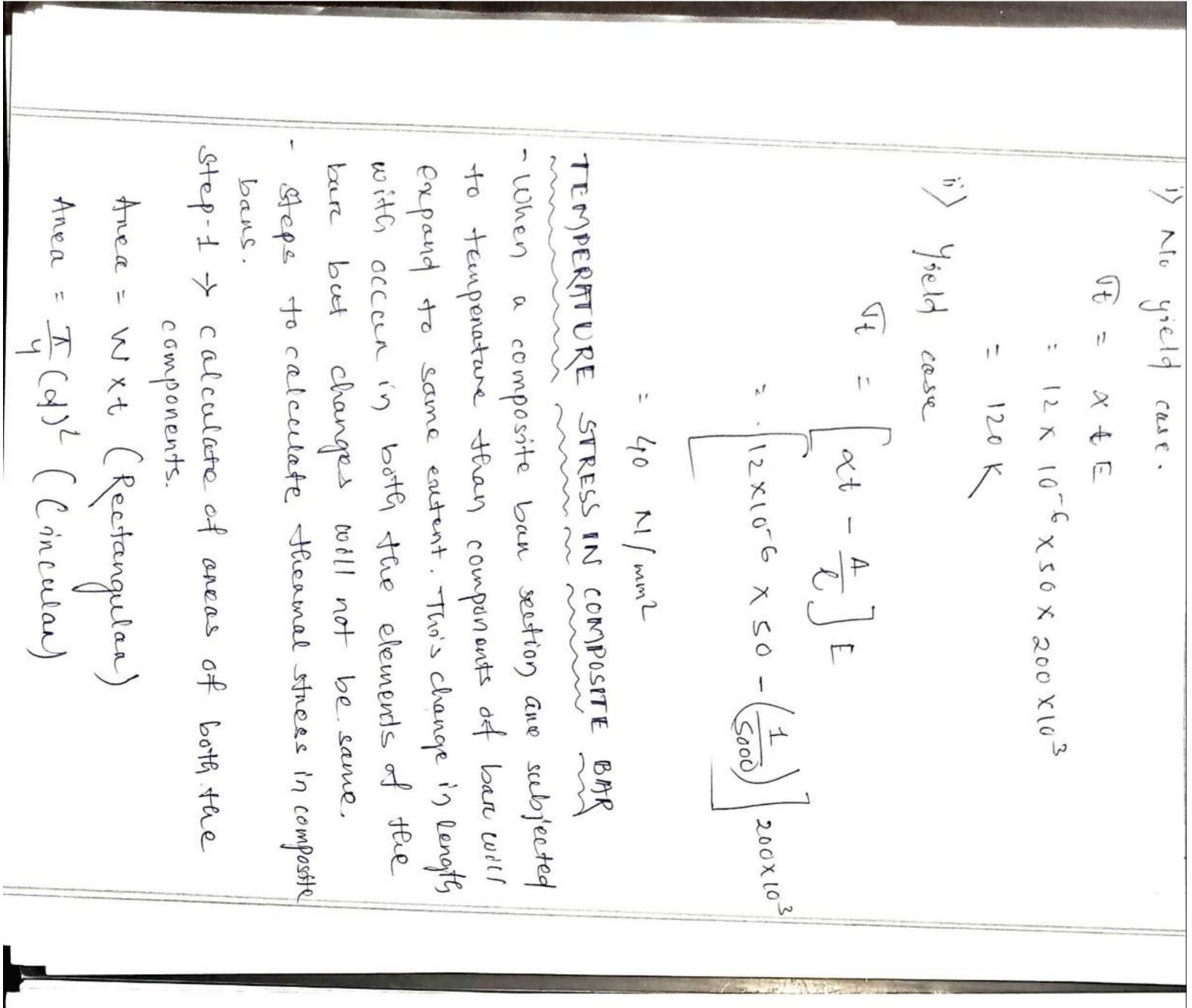
street ban fried at both ends. It head

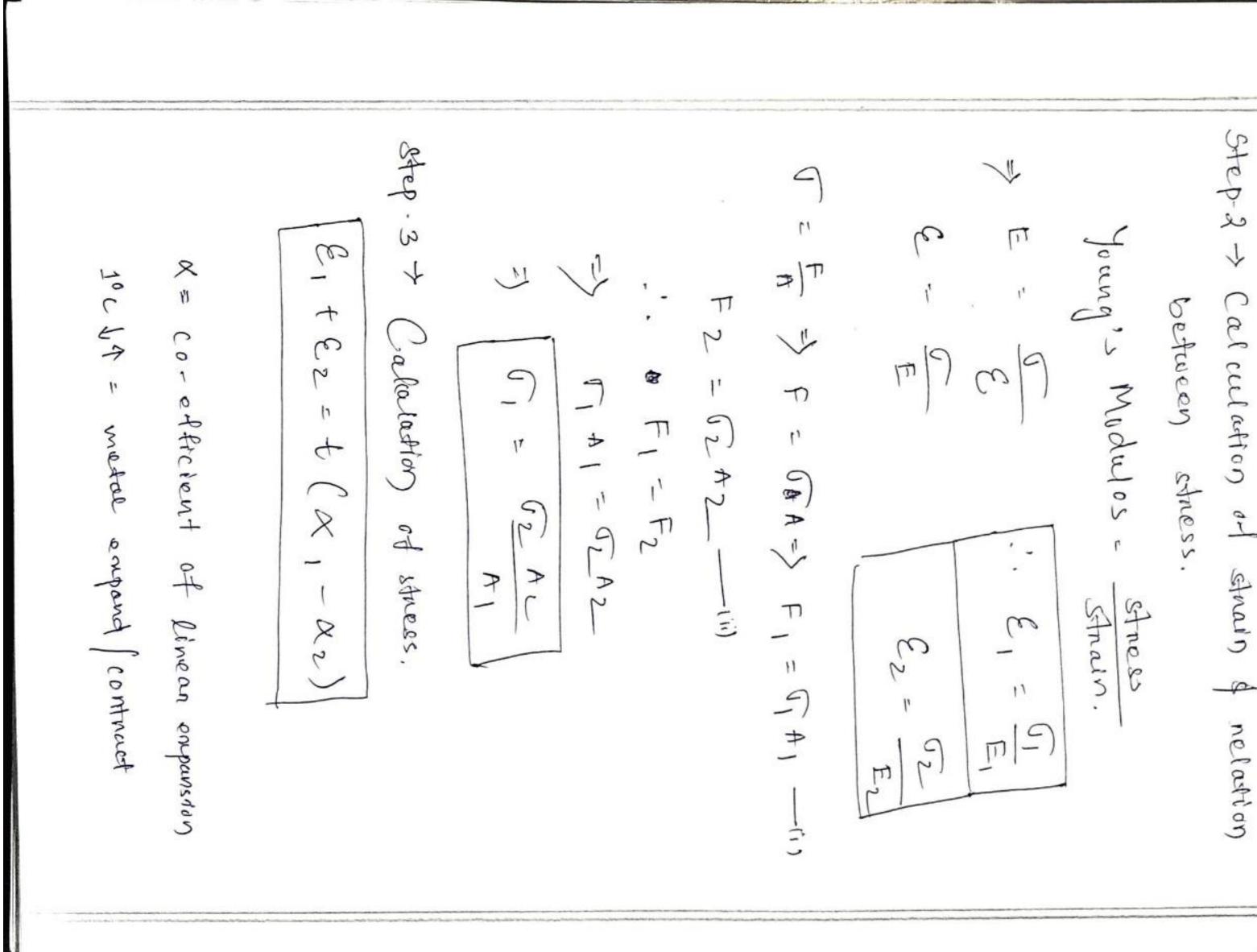
in the ban. If modulus of elasticity a

co- efficient of linear expansion acres for

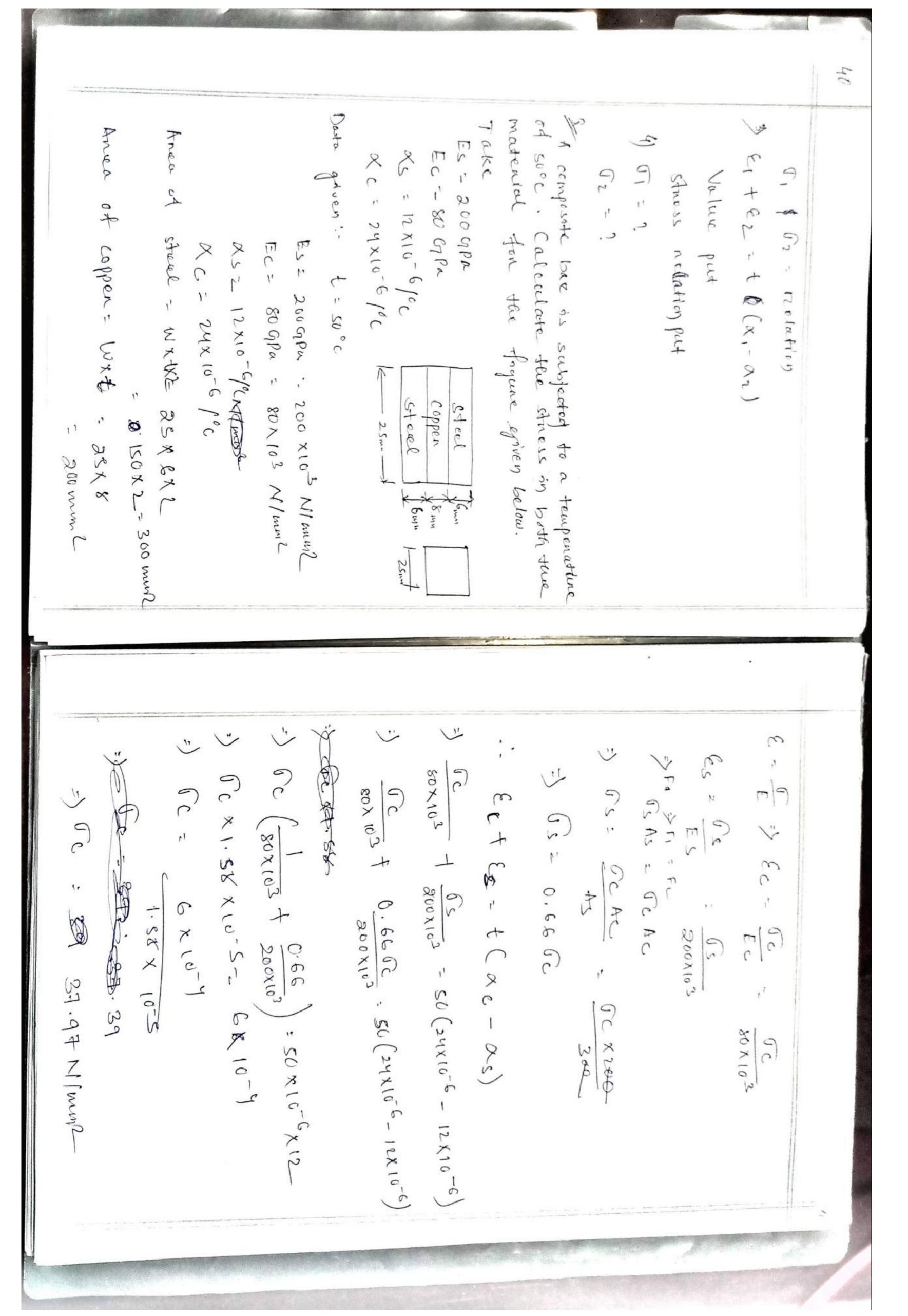
mouterial is

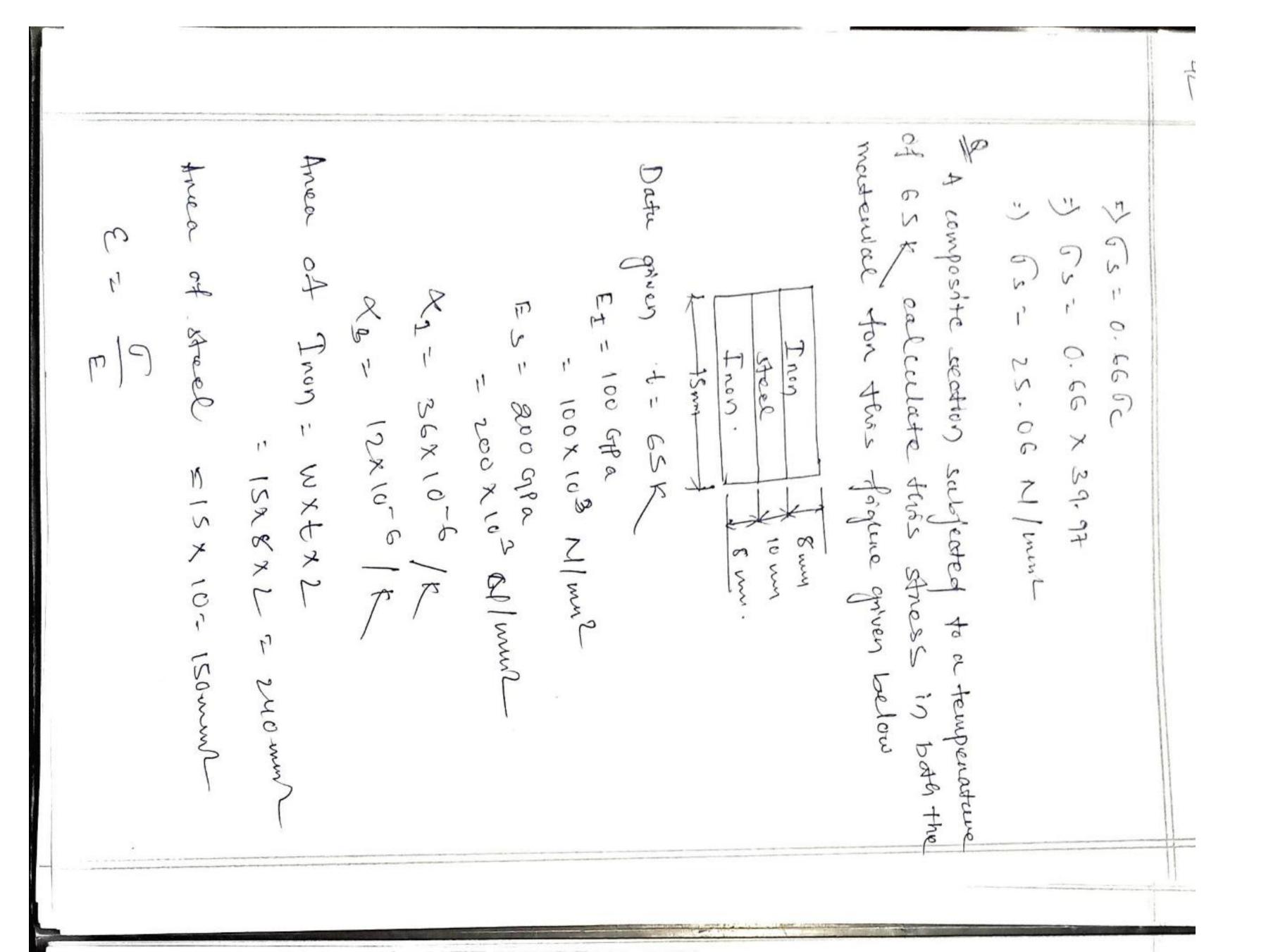
200 9Pa \$ 12×10-6/K





This is to the services of the





50500.0

0.6251 138.66

86. Ef 1/ min2

energy and when the deforming force is remove and it is again required by the eleatic body to reguined by the eleatic body to evended stored in the STRAIN ENERGY clastic body is loaded. It stones the the elastic body is known

RESILIENCE

carled as Reselvence. The strain energy stone by the body o's

PROF - RESILIENCE

The strain energy per unit volume is known The total studin Energy that can stoned in MODULUS OF RESILIENCE is Known as proof. Resildence

Modulus of resilience strain Every

- hbrows Growfo

strain

Volume

9000 N .m.

242 X105

enengy (v) G2

2000 x 2000 - 4000000

= 30 N/mm2

2000

Voleumo =

AXX

(Case-1) energy stone in a subjected graduet load. re waym Apog Volcume.

strain enemy (U)

Calculate 4) Modulus of nossitione = U(strain enemy) E = 200 GP.a Volume long. Having somm width and home.

H subjected to a load 60 KN. To govern: -AX C 92 Anca X Length × Volume 3 Lower 2 × 10000 = Volume. 2000 thick

TXW = 3 50 KZ 1 50 X102 50 x 40 => W= 200 Gpa = 200×103 N Z

subjected Dafra griven tength, of the rod 1 m. Take E= 2000/2 mod of 15 mm TOKN - TOXIOS Z 15 MM 10 KN. Calculate diameter is a

L- 1m - 1000 mm.

HIE. 9+1= (SI) x PT = 176.714 E - 200 GPa = 200x 103 N/mm2

トトラセー 1 SC. S& N/mm

176710 cmm3

Ameax length

(88.88)2 2 x 200x 10 3 - 火 1平6年10

1414.25 M. M. M.M.

applied loud of 1000 N. (alculate the struennyy stoned in the column if the longth column is am. Take E = 2000/la and 10 mm starchness is subjected to a sudd

Griven dasta! -

mm 01

1 1000Z

2 x 1000 = 2000 mm

200 gla - 2×105 M/4

& BX HOW WIGHTAX Juscenes 20×10 - 200 mml

Anna & Length

2000 7 2000

400000 mm3

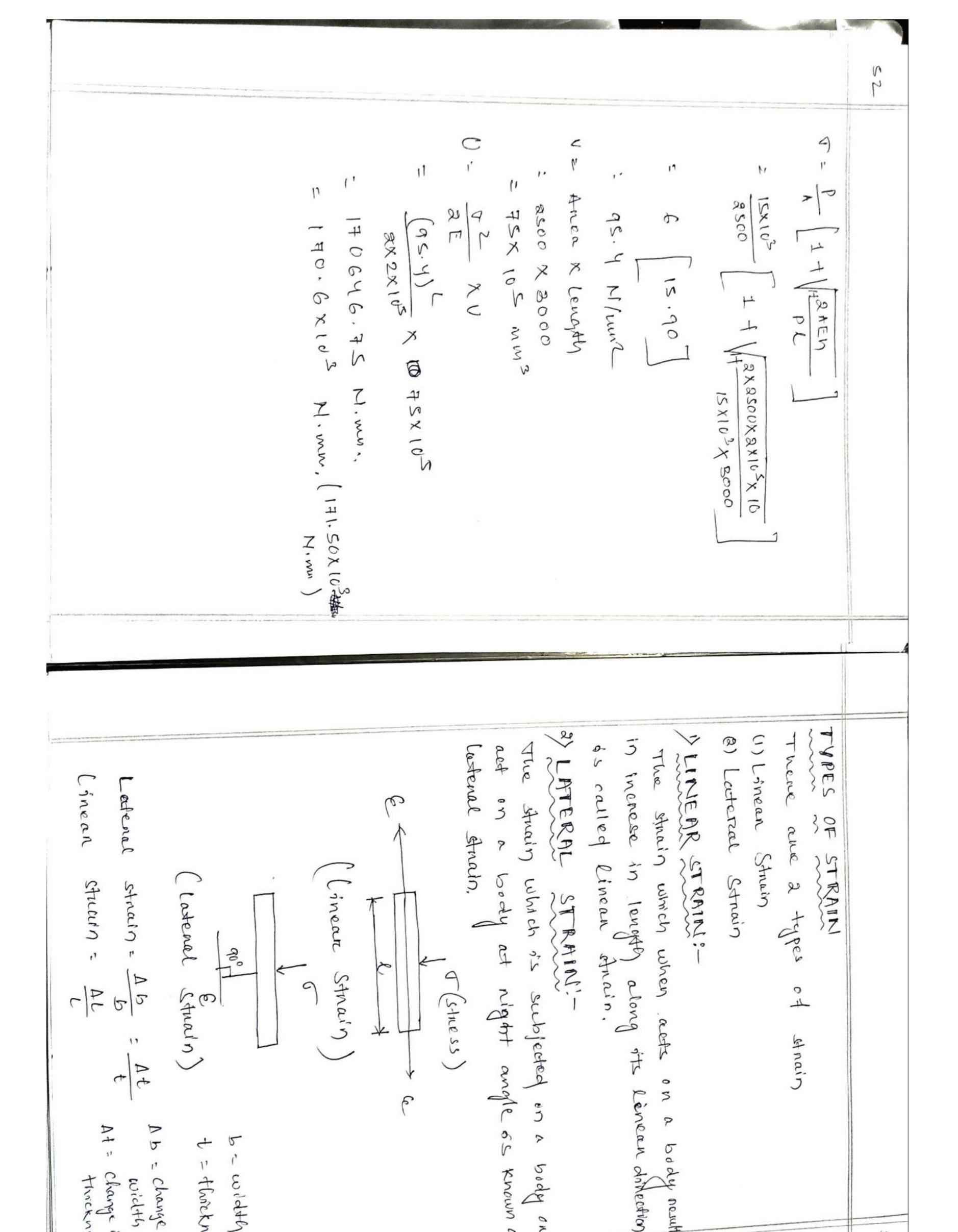
10 Jump

ENeway - 02 ax 2x105 X 400000 (M)

100 M.mm.

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4 Namus 10V rain enemaly steel bour Opiven dasta: enengy (W) = 02 xV DEPH Aneax length 1500 × 2000 2 K 12×104 Kax103×100 3×106 mm3 126.49 N/mmL to a impaced ward of 15KM height of 10 mm. Calculations the body. Tak 3 my long and \$ 2500 mm2 1 1500× 2000 (26. 49)L 2×12×104 ×3×106 199996.50 N.mm 2500 mml QUOGPA -ISKN: ISXIO3N 20001XE 2001103 2×105N1



lateral Strain mano -Arrain - Ab in width (Ab) 0.32×50 Casterial Strains 6 8x10-4x50 = 0.04 mm. with Lincan DB - = 8 X 10 - 4 CHUUD) (heart)

coad aso KN. Calculate

Young's modulus.

Paissions radio

Change in Atrickness

, Al = 0.6 mm, Ab=0.

stead bun 60x80 mm à subjected \subseteq (3) Cyhven Poission's Rasto = Change 19 Hanckness (At) afenal strain = It I I wear street 1: (ustread streets). AXAL Lastenal structurat Lasterial 40x20= 800 mm2 Linean 1.25210-3 HO WW. 3 × (0 0-05 mm. 2×10000 strain. Humps 25×104 11 0.6 2000 0.05 O02.00

01x Eh 5102040-S 5102040, 81 x 35000 5102040, 81 x35000 37 993, 92 35000

1.96 X10 3 m2 (d)2 (0.05) 1.96x10-3 5102040.61 N/m2

when subjected to a body nesults into different section.

STIEAR STRAINS:-(p)

produced in the body due to shown stress Mr. O.R: -> (G/C) -> H can be defined as the nation of stream stress to shear stress.

ased to measure the constant are the strain = Anength of a constant which ,

(9/C=

Shean Amoss

- = (N/ min

(a) Houng's modules (k) (3) Modules niggo (b) Bulk modules (k) 3 type of clastic constant.

panticulen material.

SHEAR STRESS: - (Z) (TOW)

MIDDLES OF RIGIDITY (G/C)

Shoon shoos can be defined as the co

(3) E= 6 (2) K= 0 (5) 9= 2

PAILURE

PRESSURE

VESSELS

THIN CYLINDER

*The cylinders having thrickness less than to the the dramesters are known as their cylinders.

*The cylinders having thickness greater tras to the to teth of diameter are known as

thick cylinders.

Sco = 50 (500 = 33 33

10 < 50 10 < 33. 33 (Thin cylinden)

When cylindens are subjected to internal pressure, this pressure exerts force on the

Walls on the effindent.

14 the pressure inside the effindent exceds
the maximum value than it results in the
failure of the effindent

Whenever the pressure inside the pressure vessels exceeds the manimum value than yearels excess place and the trees place action of two stresses. They are under the it organizational stress.

I's Longanizational stress.

1) EIREUM FERENTIAL STREBS ! - (Hoop stress)
*The stress which is subjected along the
cincumference on the diameter of the cylinder
is known as cincumferential stress.

* H is denoted as Te + Circumfenential eteress can be called by using formula

where c= cincentemential

t - tenchness of cylinder

come continuation extress can be colculated by regard formula.

63



is Langer UDINIAL STRESS:
* When the stress is subjected along the length
of the cylinder, this stress is known as

Congritudinal stress.

+ Longritudinal stress can be calculated by using formula (i-longitudinal stre

The Thy

Oc= congretudinal stress

p= internal pressure

d= dra of cylinder

t= thickness of cylinder.

of the joint es given then

* If the

efficiency

Bananitta = 12 B

A cylinder or subjected to an internal pressure of 2 MPa huning disameter 400 mm and Attackness 10 mm. calculate the hoop's stress/cincumfenential stress for the goven cylinder.

Griven data: - P = 2MPa = 2 N/mm²

d = 40 mm

f = 2 10 mm

Tc = Pd - 7 x 40 = 4 N/mm²

A tenn cylinder is subjected to an inten

A terrin enfinder is subjected to an internet pressure of 8 MPC having chameter 25 mm cond thackness 12 mm. Calculate the text Congritudinal Aress.

Given data: - P= & Ma = & M/mil

d = 25 mm.

12 mm

Pd - 8xx25 - 25 - 4,16 M/m2

Equilibrial stress fina eylinder having simm longitudinal stress fina eylinder having simm longitudinal stress of plates subjected and and & mm threkness of plates subjected to an internal pressure of 6.5 Mp. Take the ordinated that is free foint as ass. 75%.

30 mm

St = 48

DIMENSION 3 7 THIN CYLINIORIUM

19 diameter (Ad)

Thange on length (AL)

to tenckness du drameter Pressure

m - Poisson ratio E= Young's Mod

l= length of

Cylinder.

2+E

OF 2.5 MPa cylindrical than drum is made is subjected to an internal pressure length. Take Cal cuiate nastro = 0.25 10 mm strick plates. It the change in dia and poissons 800 mm in doia and am

> CIRCUMPERENTIAL STREET & we know that thow that LONIGITUI

2+6 Pd The 24E (7pd

DOR (1

lengstude Street M. STE (}

200 GPa= 2×105 N/mm2

(Oww

2 · S MPa =

2.5 N/mm2

cincumperent al

strain

Pd

SW

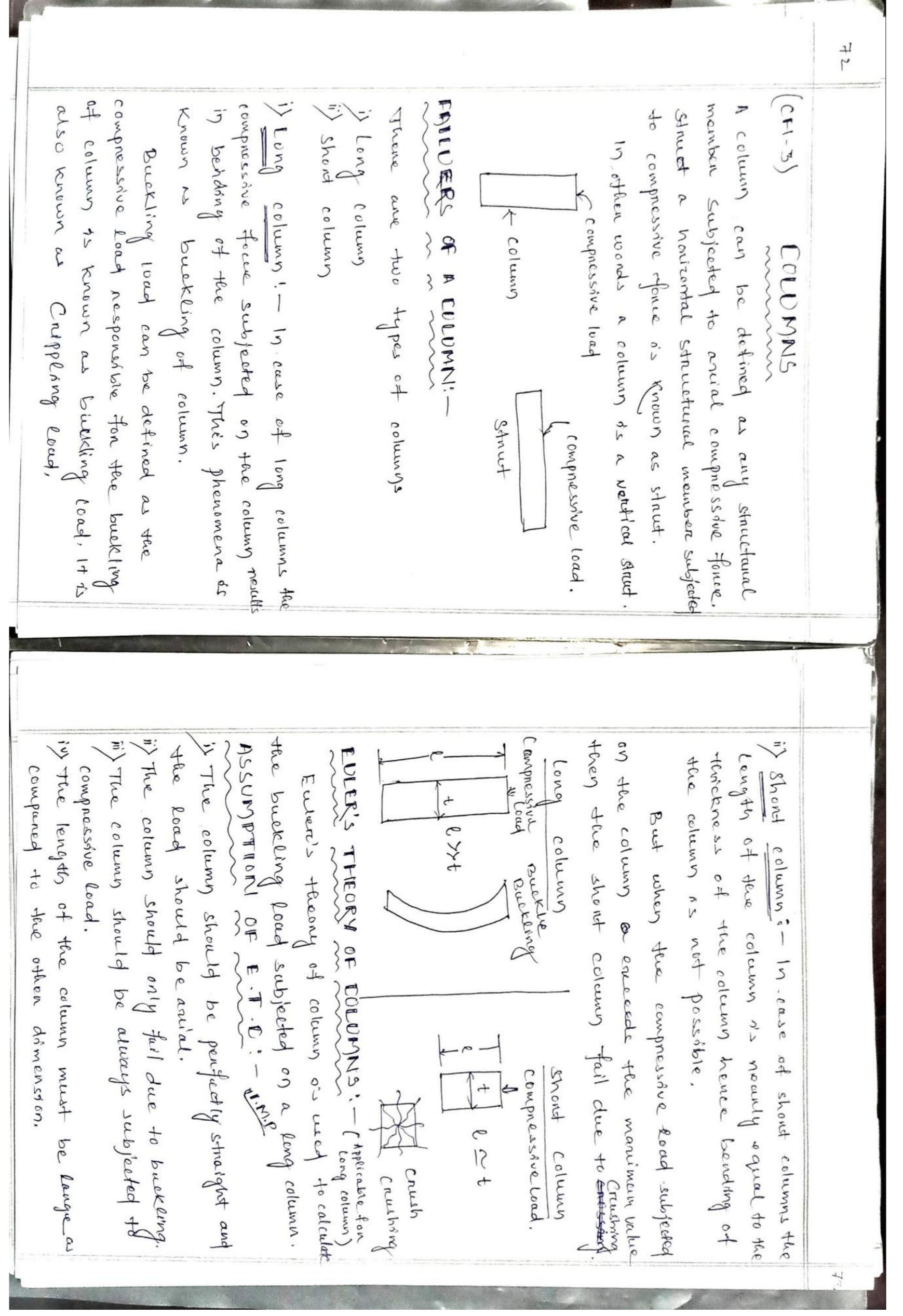
hm = 4000 mm

mm 008

PAL

2.5x 800x 4000

ax 10 xax 115 0.35 mm 2×10×2×10×



74 be uniform thoughout its longth. of buckling. The gradued length, of the column after buckling is known as equivalent length of the column, on effective of the column, END CONDITION OF A EQUIVALENT subjected to wer's theory. They are geonous When Both the ends are hinged & proned. Both the ends one Thred One end is fixed & other end is three EULER'S THEORY OF FOLUMN :column should be penfectly elastic, homo. lodi fano are 4 and condition of columns 4 Isotnopic the column as subjected to the process scottunal columns are subjected to a buebling LENGTH > throughout the column 120W anea (all properties same) COLUMN SUBTECTED OF EDLUMN! of the all purts. column should FORMULA FOR TO CALCULATE 1) Both ends are howed RELATION BETWEEN a) Booth ends are fixed END FONDITION: 1 , One end is fixed and other LENGTH OF THE EOLUMN IN DIFF other 5 > End condition CRIPCLING end as thred and ds hanged & prinned Ance Where LOAD P= buckling load on EQ. 1 Le - equivalent len - Young's modulus DSING EULER'S T Relation beston LENCHMOF BUCKLIF

& hollow diameter of Gonun and as mun nespectively was found to be entereded by 4.8 mm under a load of token. Calculate the coupplling load it the both the of cits are hinged Data given: - D= 40mm d= 25mm F - 60 EN - 6×104 N both the ends are hinged tente 4m long which external and internal 2 7 (D2 - d2) 3 ((40 - (25)2) = 34 (1600-625) 7 LX 2x10 5 X 1.866666666 (6000) 1. 2×10-3 4 00 Y 1 = 4m = 4000mm AL = 4.8 mm. 1.2 × 10-3 65291.66N/mm2 9000 33 3 5046 ends are fixed and having a change in k nectangular 4 cm data: => w= 250mm, 1= 7257 tx w ends are fixed 12/3 4288.86 N (Ans) 65291 .88 × 106488.91 *دائد* 2000 as a 40002 9×10-4 = 2222 . 22 N/am2 250x 100 = 25000 mm2 250×(100)5

= Sm = socomm, Al = 4.5mi

1,00 mm

2500 mm.

- 2083333.3

5000

Ecad Marineum column thickness Eccentucity width FULFO ecentri's and centric 25002 70 column echumn is COUMNS! 0 DIRECT which do not load is thous column the column. Column. botween) Known a ecerdic 58 cosn aide

In) for concular secotion (solid) => Z=

32 Xd3

bd2 (mm

1) For rectangular section (hollow) => 2=

1) For recturation section (solid) > 2= 2d 2 (m

The section modulus can be calculated from

formula: -

iv) for cincular section (hollow) >> 2 =

connected on a pareticular body entirely do re connected with the arrive of the body and a bending moment is known as section mode 11) Minimum intensity of stress (amin 1 - 60 SECTION MODULUS(Z):modulus modulus is provided. section modulus can be defined as the f intensity of street (max): 2 1 + 1 intensity of stress (Omin) = 1 - M P = fonce acting on column. Z = Section modulus (Fx x ds Bendring moment (PXE)

& 1 nectungular the marismum and mannamen intensity of stress. b = 1500 mm 150x 120mm it cannies a load P= 180KN= 18XICT N d= 120 mm.

150 x 120 - 180 x 103

Calculate the man

100KZ = 100x10

5 h

3

ventical load of 100 KN at the edge

and man antensity

A cinemian column having 200 mm drameter o's subjected on load 185 KN with du e countricity of tomm.

Calculate the man and min interity of Load.

(given dasta: -= 185 KN = (85 x 103 X)

1372401.47

(D2- 22)

21598.44 mm

(3002-2502)

21415.92 mn2

185XID3 X 70

1295 ×104

301x 51 = 150 mm 051 X501

3004

31.80E53E × 104

hollow chreatar & column having entend dramet 10.599 Pc.

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[TORSION)

SHIAFT: - shaft can be defined as a notating machine element which transmit power and muttern.

shaft which results in twisting of that shaft is known as turning three applied on a

TORSION / TORQUE :-

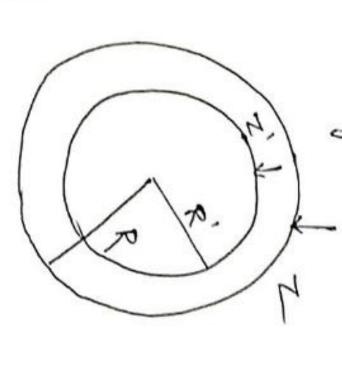
the product of turning force and the distance to the annual of the point of application as to the annual when the shaft is known as turning moment when the shaft is subjected to turning moment it is set to be in to turning moment it is set to be in tonsion I traque. [7.M = T.FX Distance]

ASSUMPTIONS OF TORSION:

ii) The twist along the shaft should be uniform
iii) the twist along the shaft should be uniform
iii) the the downeters before and after the
twist chould remain straight

IV) The cross-sestional area of the shaft
should remain prone before and after the
twist of the shaft.

Chiess adways constant 4 in that shaft and とからを PRODUCE case radrus of the shaft (R) properational the needs of shear st and subjected subjected nadni toa





costant

(PRESSION FOR TORQUE IN A SOLIO SHAFI

The consider a solid shaft having

R- Radious of the shaft

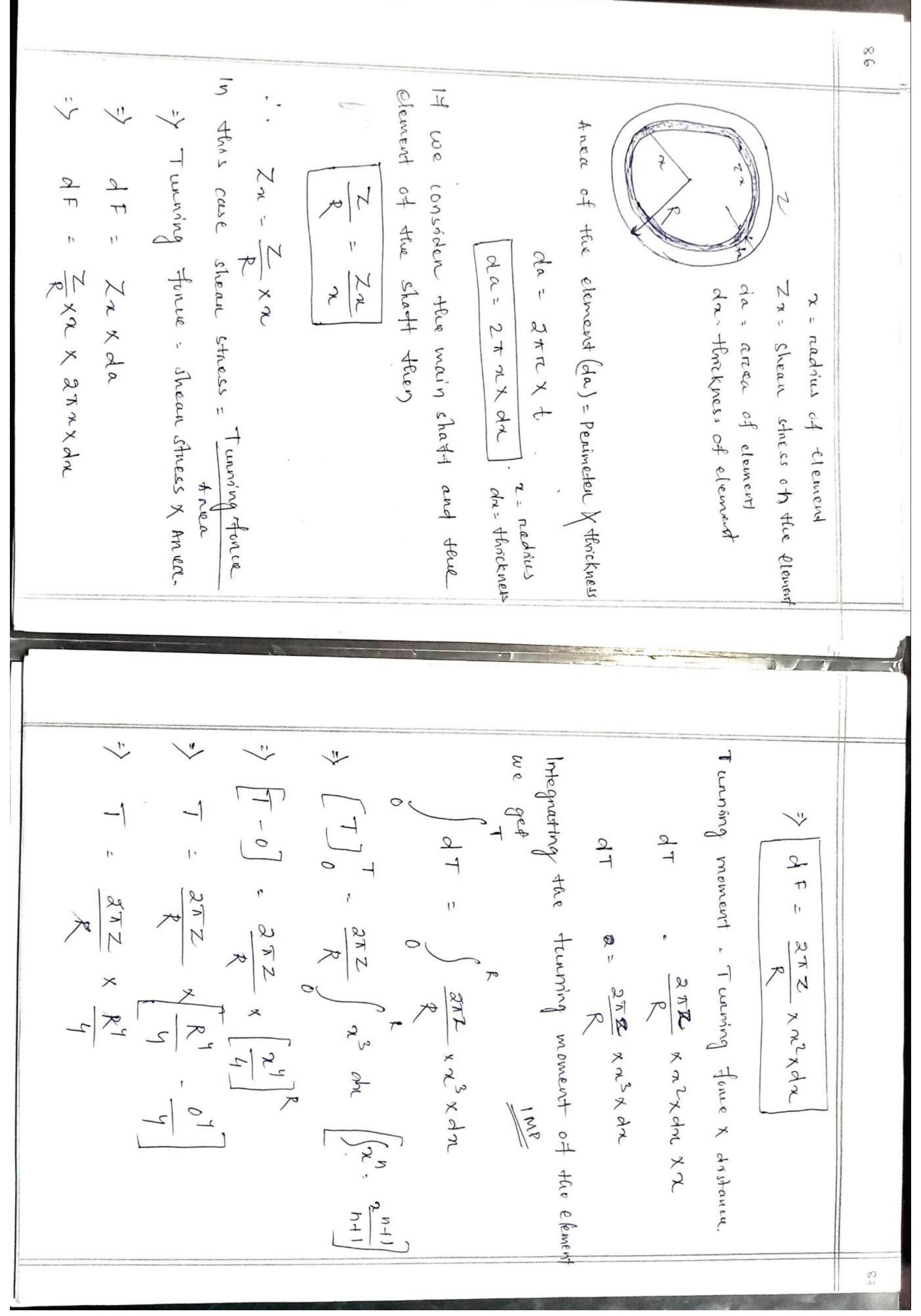
Z - shear stress subjected on the

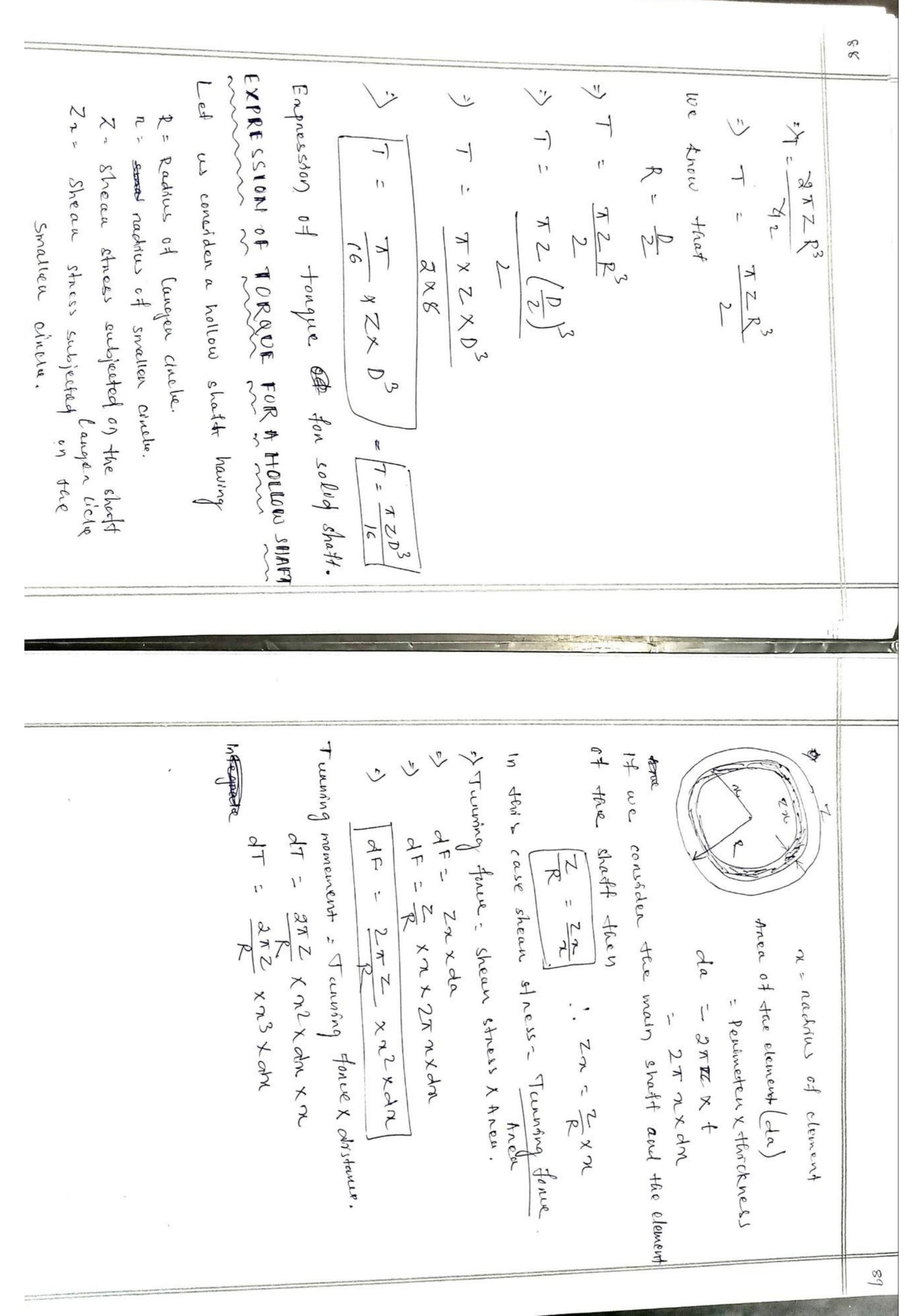
Instide howing

Intide tere shaft than It will be

Shaft.

da = throkness of element da = arrea of element





POWER TRANSMITTED BY THE SHAFT:

Power frammitted in KW

N - Speed in RPM T - Tongue in RPM

Calculate the tonque. solid cincular shaft having so my drame subjected to a shear stress of 40MP

Gren data - D - somm.

40 M Da =

16 × 40 × (50) · 17 04. 8 17 40 VI.

A solid shaft transmit a torque of 10kNm then the shear stress is govern 45 mpa then calculate the dra of shatt.

10x 103 x 103 M.mm = 107 M. 一のアス・多 45 MPa =

Indennal mal dra somm. is subjected 11 X USXD3 104.21 mm 7 X 4S X X YS 5 ا ک ا subjected

ys Mla. Cal calate the tongue to a shear shew dra so mmany transimited.

so www mm 03 45 M/mml

XSh D 4 -408

メ

33602 ·06. 21. mm

50 x (60)>

2XTX 150X 212087 10000 GO

1 *

1.

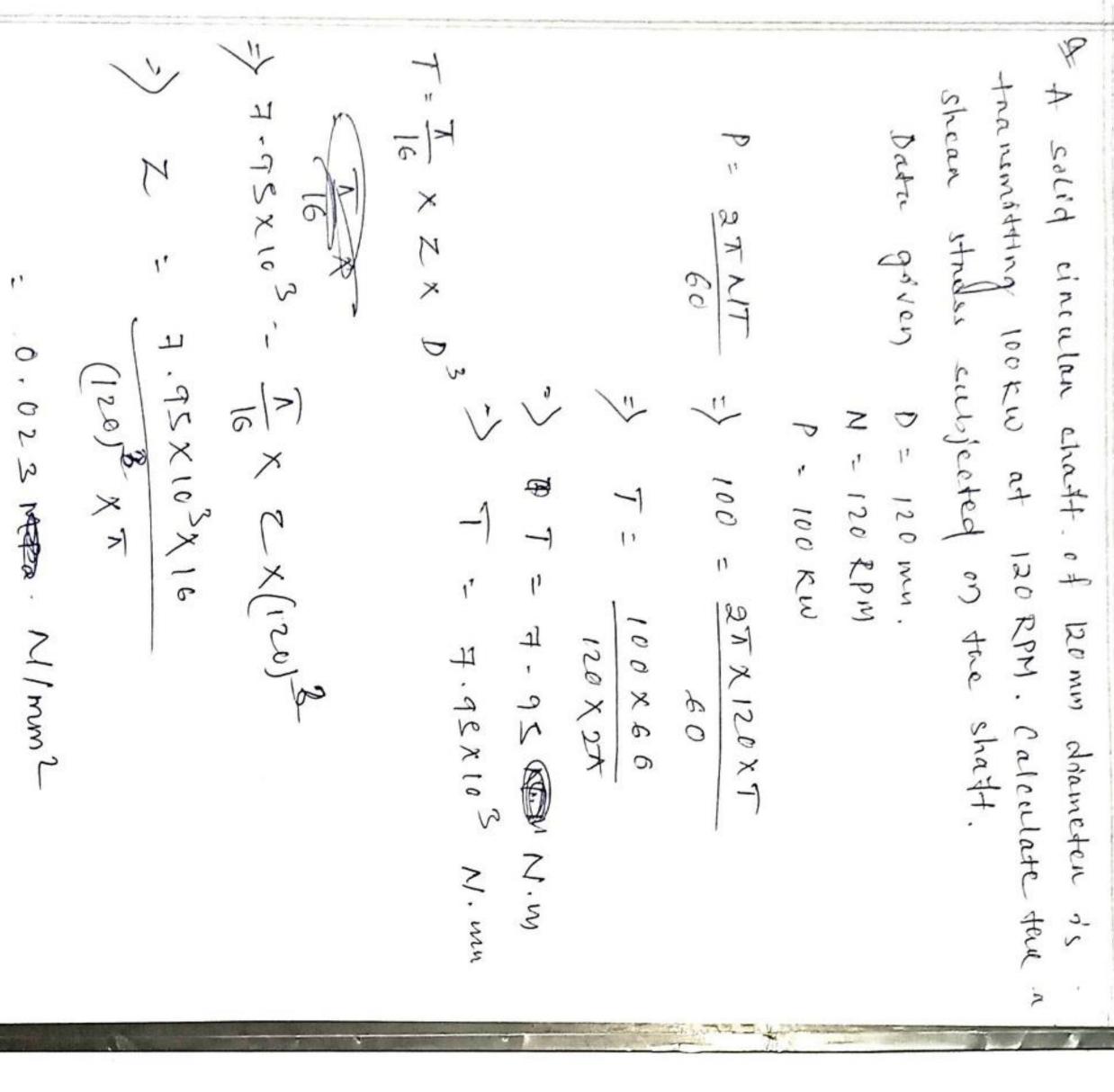
U compuny no SO MPA, 150 RPM. 14 calculate the power transmitte Alic 03 drame.

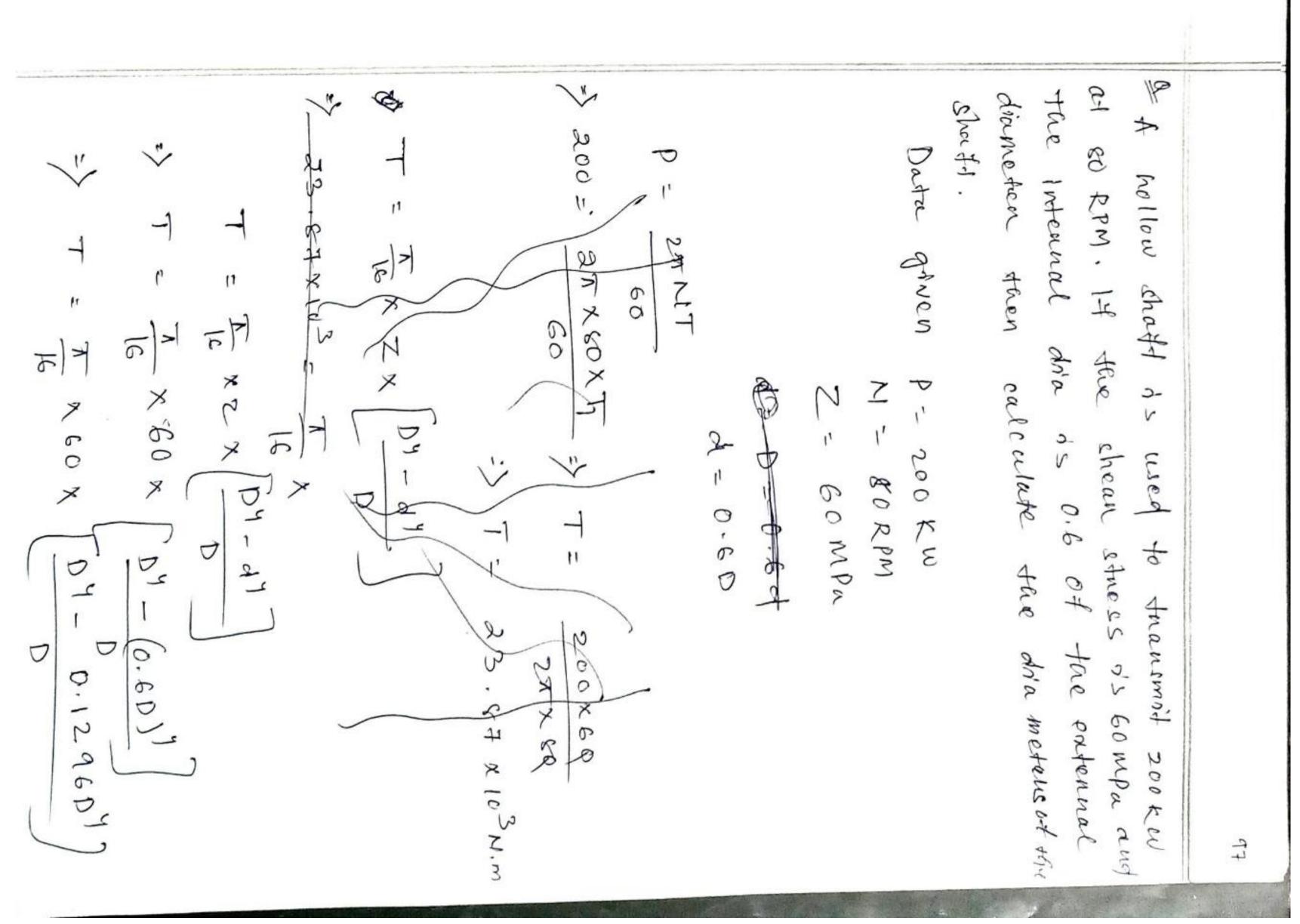
Data given

(SO RPN)

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Insteurity of shear chreas. colid 7.639x162 1 2x (100)5 16 X Z X D3 cincular 11 7839.43 NI.M. 03 x 601 x 0 81 31 X 501 X BE3- E 0.0389 X 103 shart 21 X 150 7.639 N.W 1005 100 mn, ISU RPM. M 012051 1003 X X 7.639 X 10 3V. mu. LM 0 0] drameter 7.3





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& A solud the Bath gate 160RM. 14 the Ray songhe by calculate the t_1 11 11 0 5 × 60 200 KX 60 X D3 10.25×10-3 N.m. stacel 0,6×13,25 -7.95 mm 10.25 D3 = M2229,09 x + 1 (1- 0.1296) 200266 27 x 80 x 20.25 x 10-3 p3 may shaft transmit 100 km at shear stress is given to Ma. John to Ma. X XOO = OF B X GOX TOX x 80 x 10.25 x 10-3 201. torque 40.8704 oncereds the (100 y . + 201.) Tm 5.96×103×103 46 x 10 3 x1

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110 0 × 103 W 90 RM

2727 65 N/mm2 60 × 110 × 103 27× 90

11671.36 Nim.

11671.36×103 N.mn.

1457. T mean

1.45 × 11671.36×103 - 7 means

16923472 N. mm.

6 16923472716 X Z X to D'S

REPENDING A - TAWIAS

and the shear stress are constant and eq Solid me are required to replace sume that the tongue transmo chaft. In both the of 60 mm dia o's to a hollow sha

replaced by a Chollow shoult having the inter dra of 85 mm. Calculate the enternal dra A soud steel shart Tonque transmitted hollow shortof. Hollow shutt.

XXXXX

(60) D (60)3 D4-(85)7

216000 D 216000B + 52200625 D7-21600D

replaced by a hollow shart of enterinal A solid steel shaft of 60 mm dra is to be replaced Tonque fransmitted ~ hollow the hollow shaft. by solid shaft (T) 65 rapial do 803× 100 shadt, other Internal 800 \$ 100 T = 100 4 - dy (100) 4 - dy 1007 Compat x 300 76 x/2 x/ half of the external dra. hollow Shall Determent the external 90mm Tonque fransmitted 83.58 endennal dia of the hollow hellow shaft (7) dra of 803x100 0'S do shaft 100 mm Tonque Inansmitted by solly shaft (T 603 X D = (60) 3 0,9375 0.0625 p4 17 30.65 No 1100

102

THEORY OF SIMPLE BENDANG)

the bending. It the is stops. This tresostance then When a beam bearn is subjected to a bending moment Process of moment than the process of bending tresostance às known as bendang ess of bending stands. The exoss-section of fores a newstance to the process

moment and the length of the section before Gempnession and 1+1's length theneases throw bending should not Let us consider a small length of a beam subjected to bendring moment. Now consider two section AB and CD in the section of the beam section why ch THEORY OF SIMPLE BENDING:- WAS and Junalled to the assist and RS. layer of the beam nemain same after bending. 12 subjected to to

one layer present in the centre of the whill nomin

. The bottom layer of the beam

to compression dension and it?

· length

2

AB

tension

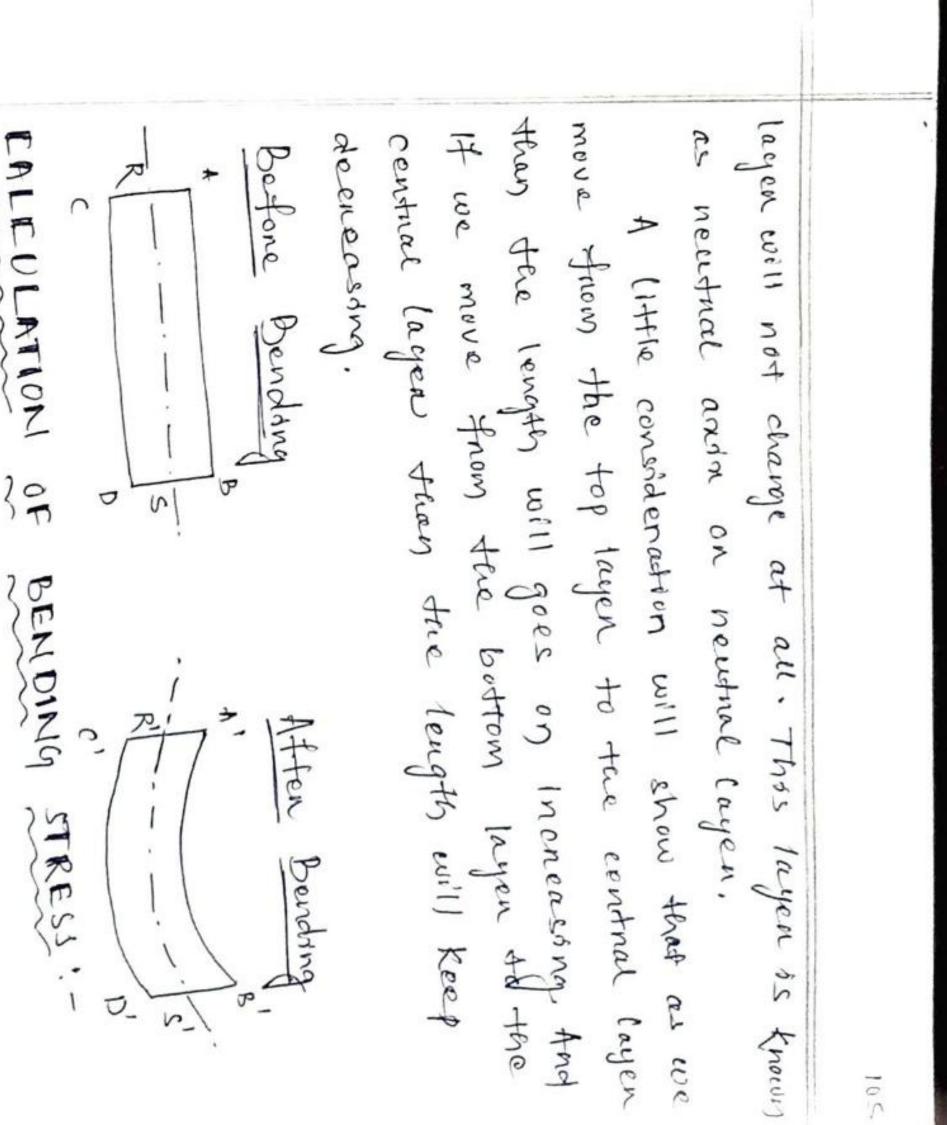
02

compression. The length of

Tart by

beau

be



Where 39 mosterwal to cover the Half of the drameter bendong stress Young's Modulus Radius of the object

[1-6) (PRINCIPLE STRESS & PRINCIPLE PLANE

PRINCIPLE PLANE! -

is equal to "zero", that plane is known as principle plane. The plane in which the magnitude of shear shou

In other wonds in priciple planes the shear

* There are various cases where spresses and priciple plane is Known as principle othesses. subjected to an snelined prime or oblique Case - 1: - (2) The stresses which are subjected on the

to oblique coeffon of a body subjected to

two direct stress. (asc-2! - (07, 04) An oblique section of a body subjected to

Case 3: - ((2x)

donest stress and An oblique seefies of a body subjected to a 8 shear stress

An oblique relation of dinect stress and a shear a body subjected to a stress

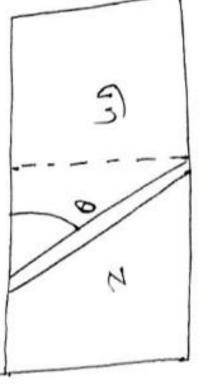
For calculating the so

Analytical method.

ii) Graphical Mextud.

i) Analytical method for Case-1: An oblique seeding of a budy sub an indined on oblique plane. calculation of it

a dinest stress (on)



upon by two stress. They In this case the

a) Normal stress (07)

Shean Aness (2)

nounal stress (69) Shear stress (2) cos 20

1 07 + (Z)2 Z= 540 20

shear others if it's makes angle of asomothy A wooden ban is subjected to a tensile 5 mpa. Calculate the value of normal stress plane.

Daten Bivers at - S MPa = S N/min2

NN - 5 COS 2x2x0

2.5 - 5x 0.64 = 0.9 N/mm/ /MPa

5 st n 2x250 - 1.91 MPa

Choss section is A wooden bour is subjected to a normal stress sample to value of fonces. Take 8:600 0.5 MPa and shear stress of 125 MPa. 14 the stresses in both 200 × 100 mm then calculate the the cases. Also calculate

govers 0-5 MPa 2 - 1.25 MPa= 1.25 N/mm2 = 0.5 N/1 mu 2

600

COS 120

2049 2.0.5 0.5x4

9

Stress X Area.

13200 N (Smallest value Stress) for

value Lauge

1.3 MPa. The cross section to 100 mm X100 mm X angle 600 with the plane then calcula wooden ban is subjected to a shear

Data grow i) structs 1.3 N/mm2 - 001x001

Sinza sin 1200

Stress & Area

(ase-2: An oblique seelin of a body subjected Hwo dineed stresses. Monumal stross RO1 10A Da-94

a) shear stress 1 0 m

Resultand Stress OR: VOM2+ Z2

4) maximum shear Shess

10 - 00 76 D

two tenselle stresses of stress for an inclined seed on of a body subjected to Determine the normal stress, shear stress, resultant 200 MPs and 100 MPs macking plane.

an angle of 300 whith dhe Dasta given Pa - 200 M/mm2 300 100 N/m/2

> SAN 2×30 200

43.30MPa

It in snowined seedles if a bidy making an angle Calculate. On 2 or 2 max also calculate of median of negation of stress. 6 R= V(125)2+ (43.20)2 = 132.28 MPa. 100 MPa acid a compressive groon MOS to searts

(or = 100 mpa

1 >5 coss 6 יון 23, 20 MPa

(-23.2)2 + (57.45) L= 100 \$ 56 . CAN \$00 - 57. 45 MPa 61. 99 MPa

Dencetor of acceletant doness

deal of 2

trans = 2

tr

Data given 0 - 51°

On = <u>300</u> - <u>100</u> cos 110°

- 100 - 50 cos 110°

Z = <u>000</u> 100 sin 110 - 46.98 MPa.

T = <u>100</u> 50 sin 110 - 46.98 MPa.

OR = $\sqrt{(117.10)^2 + (46.98\% - 126.17)}$ MPa

Zmax = + 180-50 = + 50 mpa

Ho a dinest editers and a shear stress.

3) Normal chaese

(h) = (1) - (2) - (

angle of 20° with the plane. CHACLES . element i'n a body o's subjected to a the of as' of as' of as' of as' o'n the clockwise dimention making on the on Data Given Tre 100 N/min. 11.98 MPa/N/mon 100 sinyo" - 25 cos 40° 4. 37 MPa on M/mm2 - San 20 - 224 cos 20 - 100 cos 40° -(50)2+(242 82 mys haz - 82502 0 25 x 547400 subjected to a fondle

tan) OB @ (SX) + (Eso)2 . SY MPa. 50 60520 + 50 Cossa 08 ULS 05 P C

and by along with S

= + tan 20 a = 9x 2 xy

= + tan 20 a = 150

=

An element is subjected to a compressive stress of 200 Mpa and a stockwise stress of sompa. Making an angle of 35° with the place calculate by, 2, 2 max

Data John Da - 200 M/mm (

- 200 + 200 cos 70 - so son 70

Z = 00 - 200 SANHO - SO COS HO

-112.78 MPa.

Zmax - ([C100) - + (50) C

1) 2 - (2 - (2) + (2 - (2) - 2 24) cos 20 - 2 24 es

Denservon of Zmax

tan 20n - Trans

of 250 mpa and 100 mpa making an angle of 20° closed wise dinection, calculate on 25 mpa in the

Data govers (2 = 100 N/mm2

D = 100 N/mm

350 - 250 105 40° - 25 cm 40

101. 47 mpa

119

dinect

stre ss

and one

shear stress.

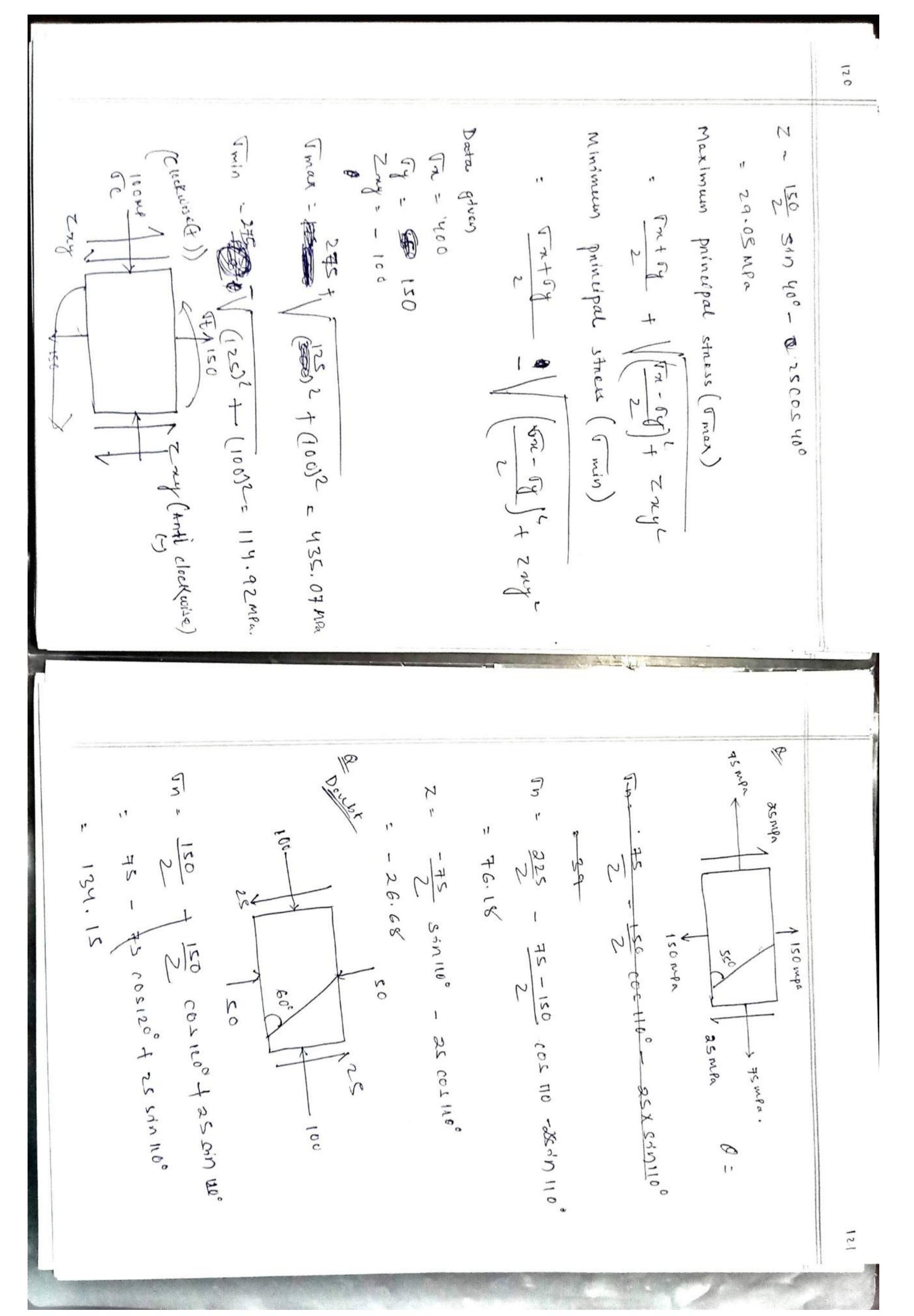
An

oblique

section of a

body

subj



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-100 +50 5 COS 1200 60528 COS 20 120 +25 Sán 120 f 25 SANI200 - 224 Syn28

18-59-

100456 SAN 28 Sanloo STATED - 25 COS 120 - 2my cos28 - 25 cos 120°

GRAPHICAL METHOD FOR CAUCULATION OF STRESS

evaluation of principal stress and principal strain. MOHR CIRCLE OF STRESSES! - It is the graphical Representation of stresses. In other wonds it can be defined as the graphical mestrad used for the

Case-1: - when the inclined body is subjectes

to one dinect stress.

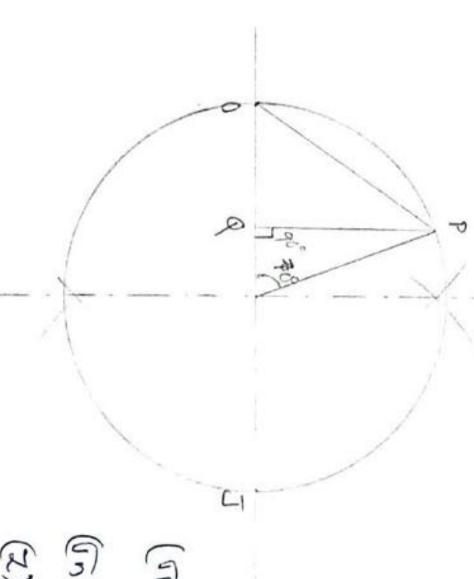
Cud '03' lest towards on right. Lest of a point 0' and dnow a line through it. right equal to the stress Jowards night compressive - Ather point.

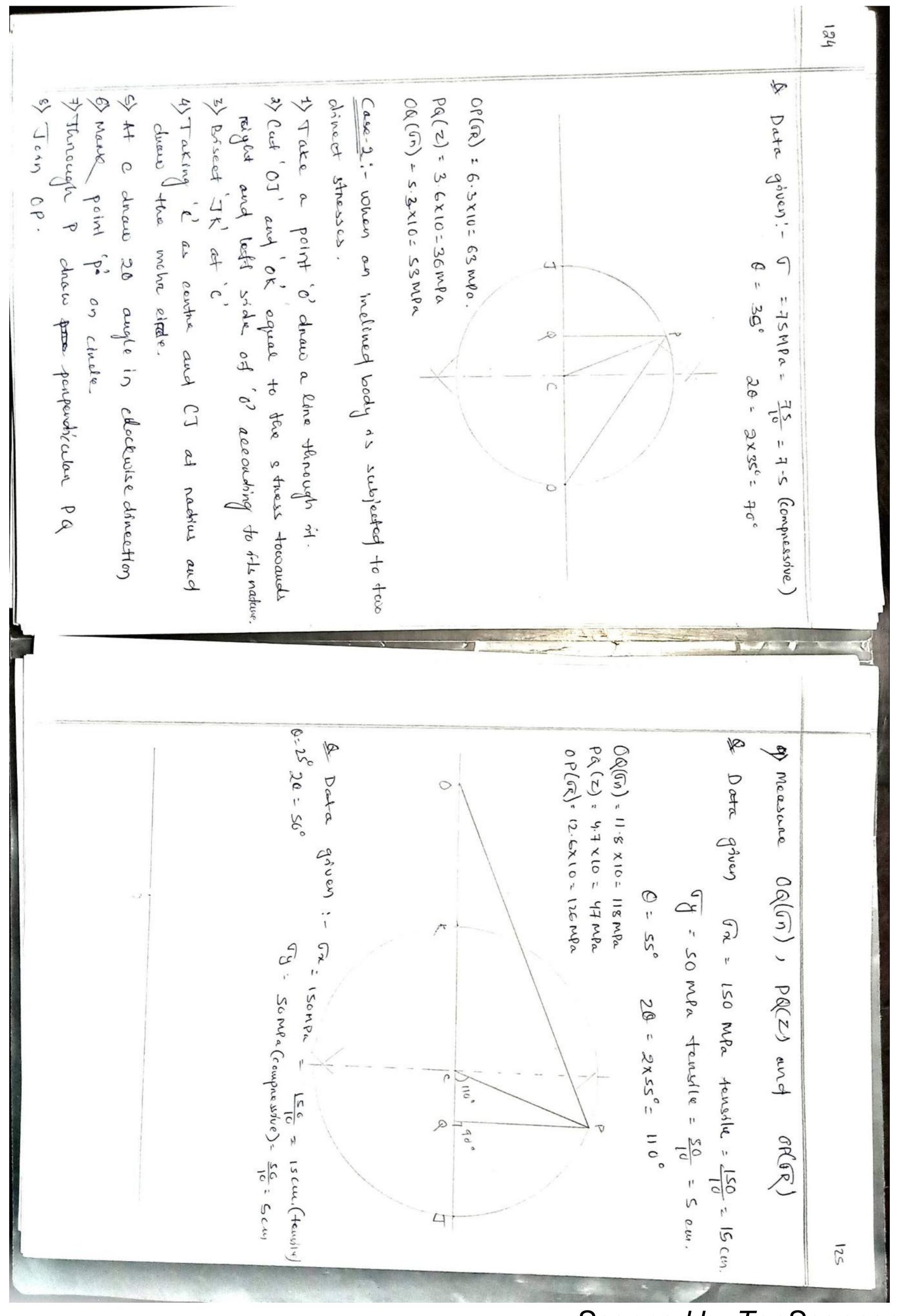
28 angle

dinection.

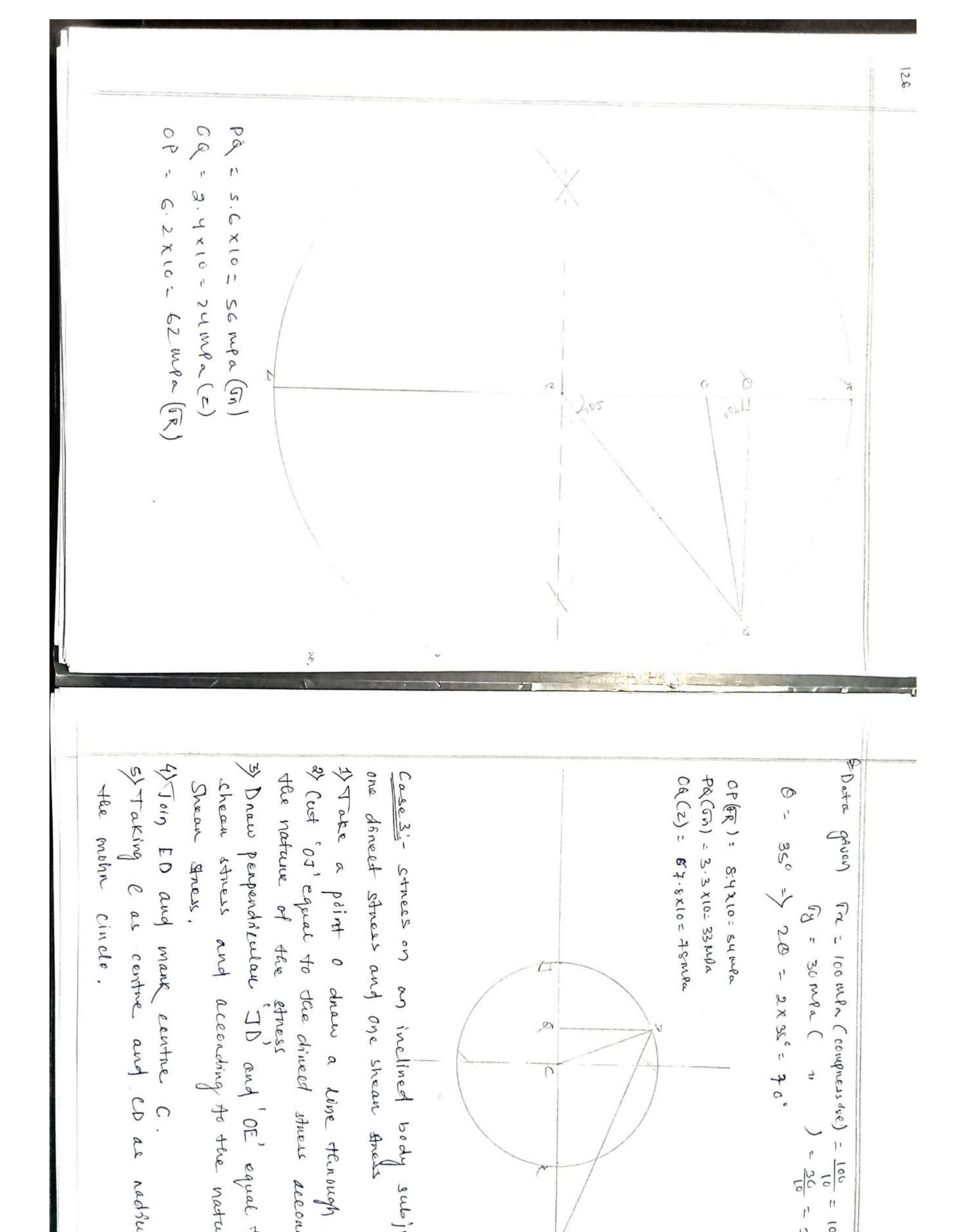
perpendscular

normal





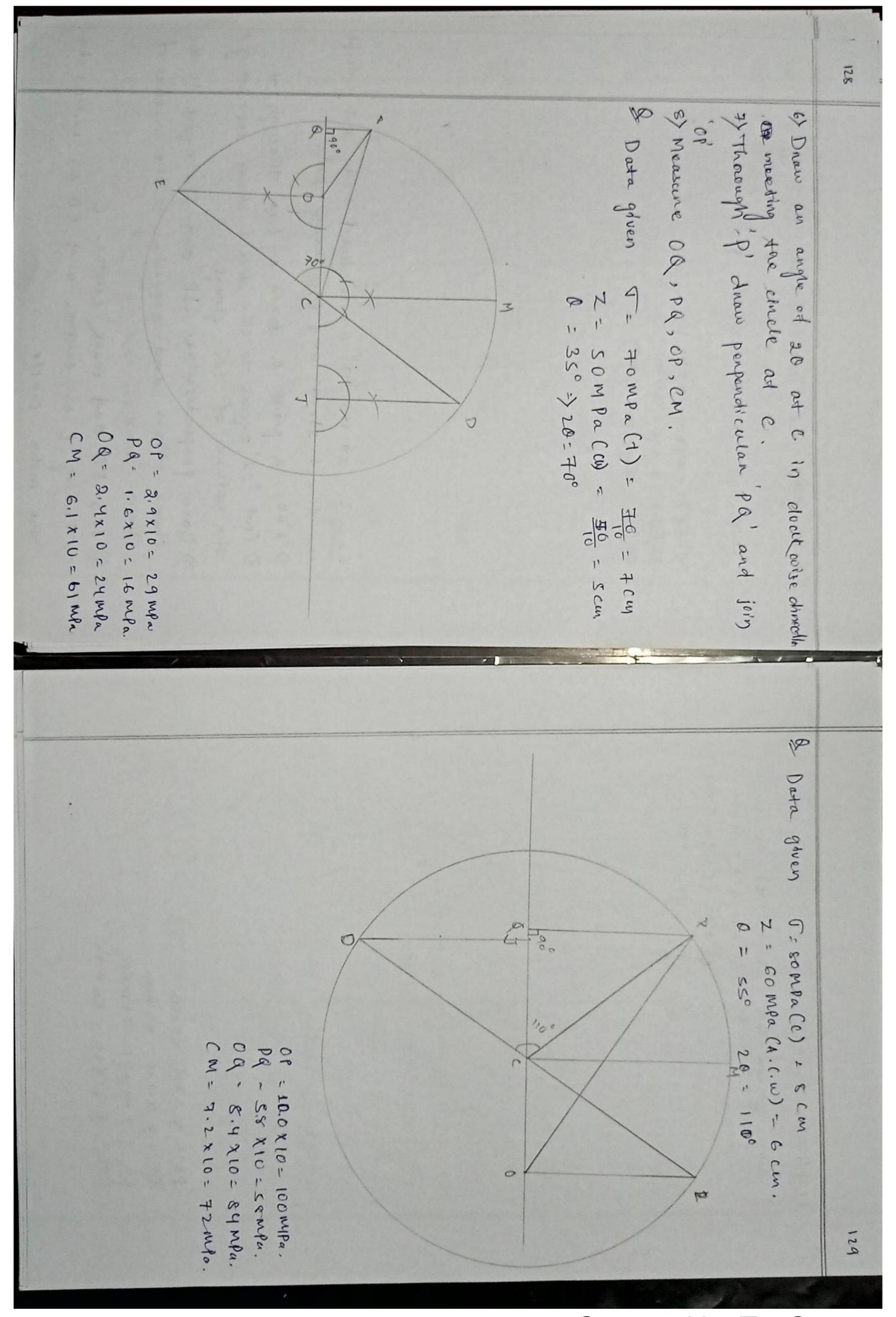
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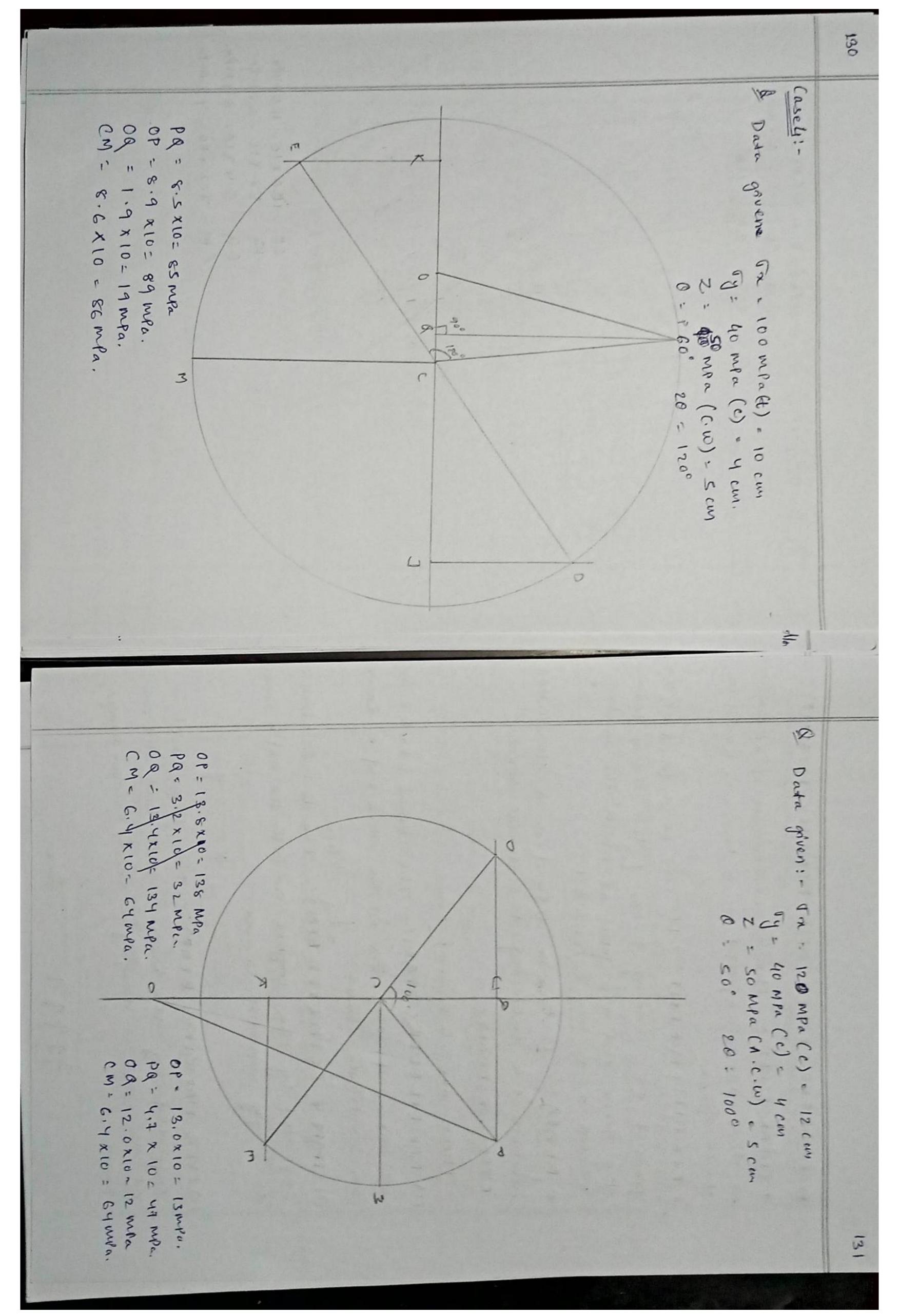
one donnect stress and one shear stress

PQ(Gn) = 3.3 x10= 33 mpa CA(2) = 87.8×10= 78mPa 100 mpa (compness ove) 30 mga 10

3) Draw perpendicular s) Taking e as centre and eD as shear stress and according to the natu ED and mark centre C. of the etness and OE equal to the



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(H-0) SHEAR FORCE AND BENDING MOMENT

* SHEPR FORTE: - The algebras sum of all the force subjected on a beam is known as

the force and the point at which the bending product of bending funce & the distance between BENDING MOMENT: - 1+ can be defined as the

moment is to be calculated.

members i.e subjected to outernal fonce TYPES OF BENN BEAM! - It can be defined as a structural

There are 5 types of boom.

as cantileven beam. The office beam which is (1) CANTILEVER BEAM: - The beaun which is fine

as samply supported beam. supported by the support on both the end is known

(3) OVER HANGING BEAM): - The beam which is suppristed by the many supprists but still one of its ends is hungary is known as over hanging

(S) DONTENIOUS BEAM, :- The Supported both the by many suppounds throughout it's BEAM) :ends Known beam which is

07 CORDING

on a point. Points load => The lossy which is ane Is type of louding subjected on concentrate 2

3) Unitonin dristuibuted subjected privational Load & (UDL) + The , scot i'an load 4

3) Wanying Load & The Coad Chempong venying load. which magnifule

